

Demonstration of an Energy Efficient Lunar ^3He and Volatiles Extraction System

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NASA Space Technology Fellow

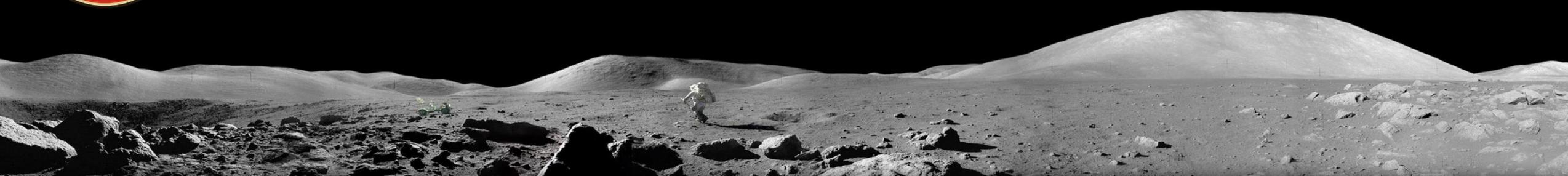
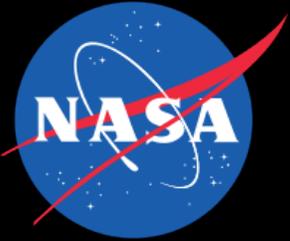
Fusion Technology Institute

University of Wisconsin-Madison, Engineering Physics Department

Planetary and Terrestrial Mining Sciences Symposium

Canadian Institute of Mining Convention

Montreal, Quebec, Canada May 13th, 2015



This Research is Supported by a NASA Fellowship

- Space Technology Research Fellowship (NSTRF)
- Class of 2014
- Collaboration with Kennedy Space Center



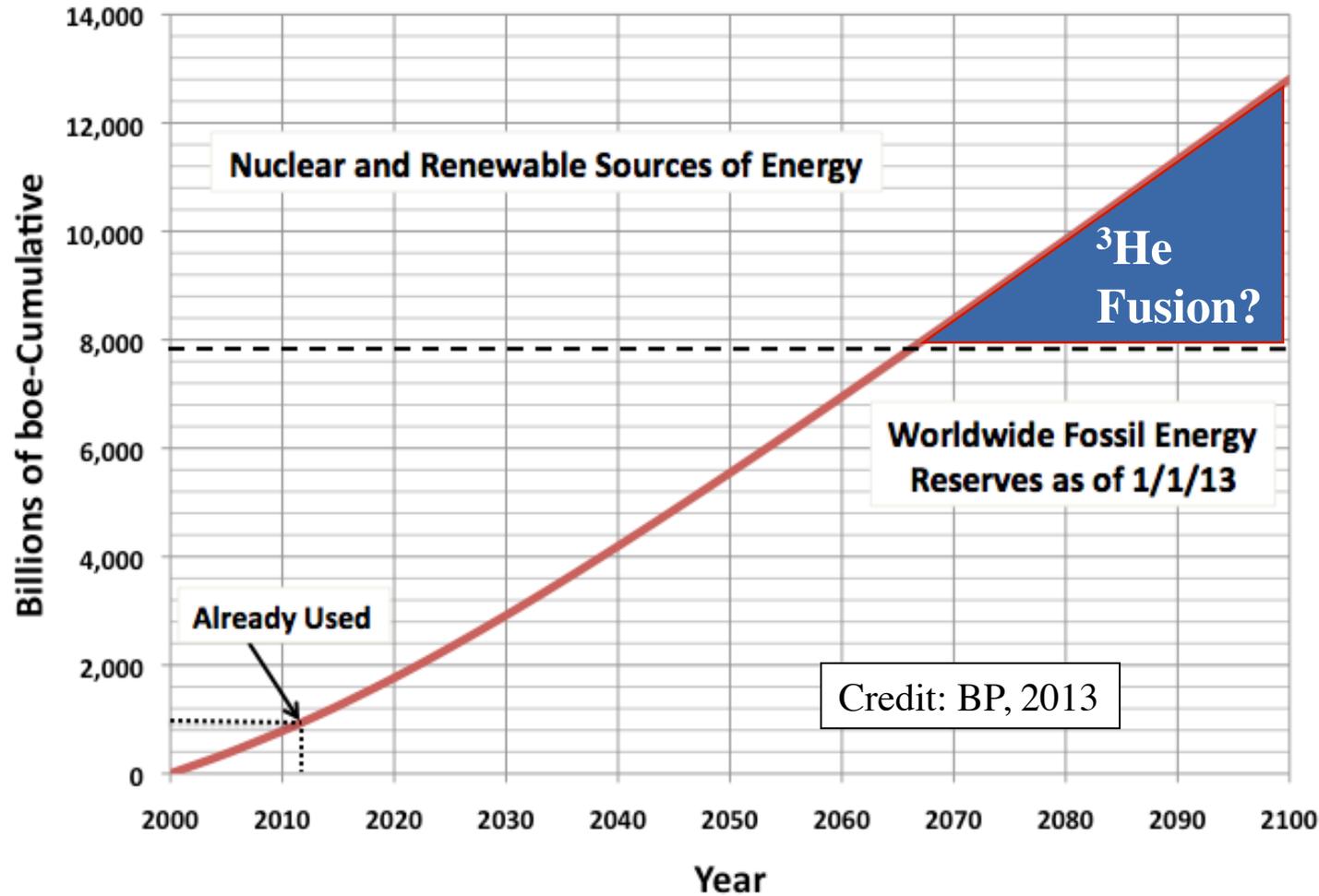
The screenshot shows the NASA website interface. At the top, there are navigation links for NEWS, MISSIONS, MULTIMEDIA, CONNECT, and ABOUT NASA. Below these is a search bar and a secondary navigation bar with links for 'For Public', 'For Educators', 'For Students', and 'For Media'. The main content area features a sidebar for the 'Space Technology Mission Directorate' with various program links. The main article is titled 'Lunar Volatiles Extraction Technology for Future Fusion Power and Multi-Outpost Scale Human Space Exploration', dated December 8, 2014, by Aaron Olson from the University of Wisconsin, Madison. The article text describes a prototype lunar volatiles extraction system designed to acquire helium-3 and volatile gases for life support in future fusion reactors. A portrait of Aaron Olson is shown to the right of the article text.

Outline

- Motivation for using Helium-3 (^3He) for Fusion Power
- How can ^3He be acquired from the Moon
- Ongoing Research to Demonstrate Lunar ^3He Extraction
- Conclusion, Expected Outcomes and Future Work

Motivation:³He Fusion Could Help Satisfy Future Energy Needs

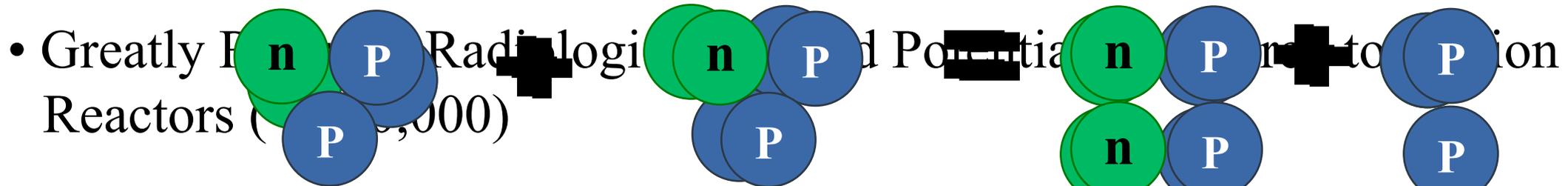
- World population is increasing
- Energy usage per capita is increasing
- Nuclear and renewable energy will be key in meeting our future needs
- ³He fusion can be a part of the solution



³He Fusion Reactors Could Produce Nuclear Power With Little to No Nuclear Waste

- No Greenhouse or Acid Gas Emissions

- Very High Efficiencies (>70%)



- No Possible Offsite Nuclear Fatalities in the Event of Worst Possible Accident

- No Proliferation of Weapons Grade Material

Deuterium + Helium-3

Deuterium (${}^2\text{H}$ or D)

Helium-3 (${}^3\text{He}$)

3.67 MeV 12.86 MeV 14.68 MeV



^3He Fusion Reactors Could Produce Nuclear Power With Little to No Nuclear Waste

What Needs to be Done?

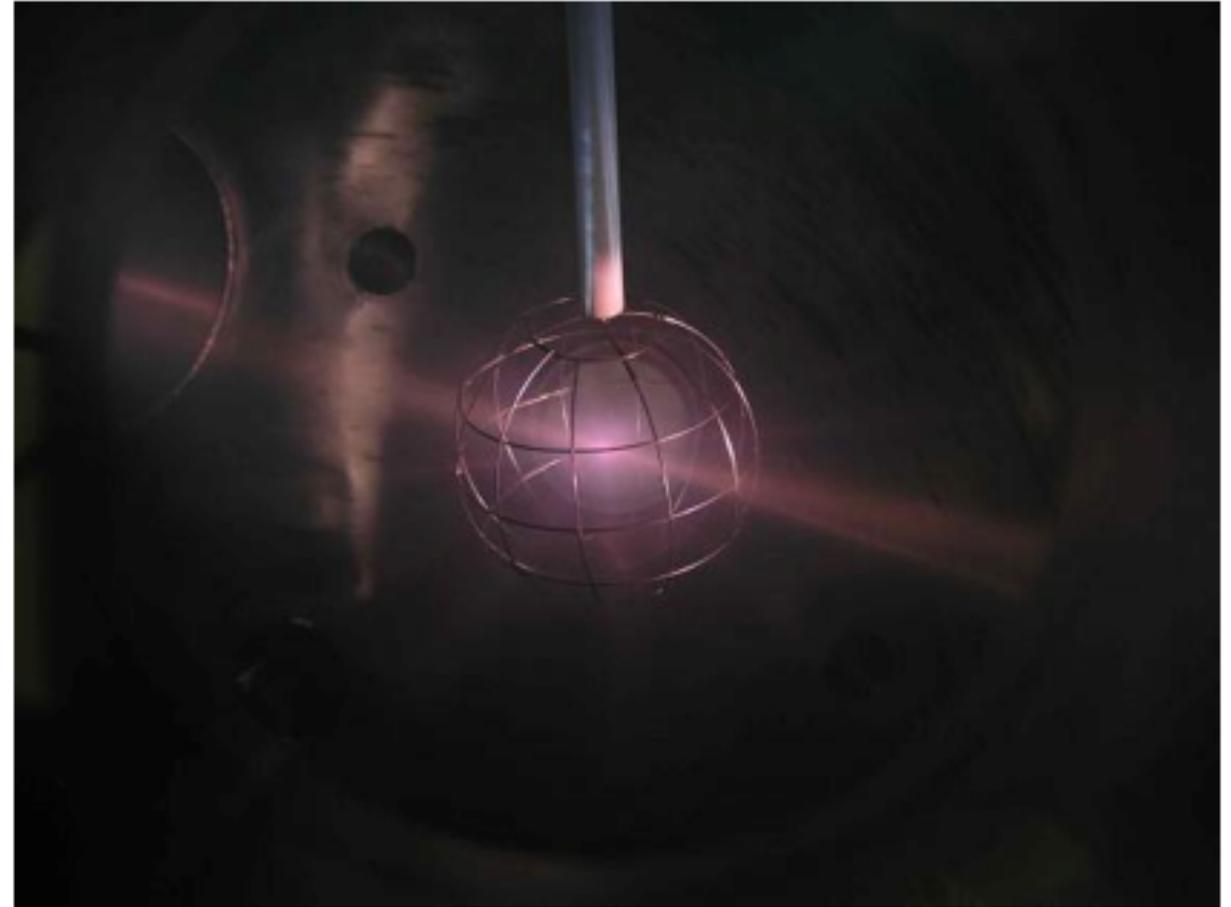
- ^3He Fusion Physics Experiments
- A Large Source of ^3He

Progress at Wisconsin Toward ^3He Fusion Reactors

D^3He fusion reactions in an IEC device demonstrated in 1999



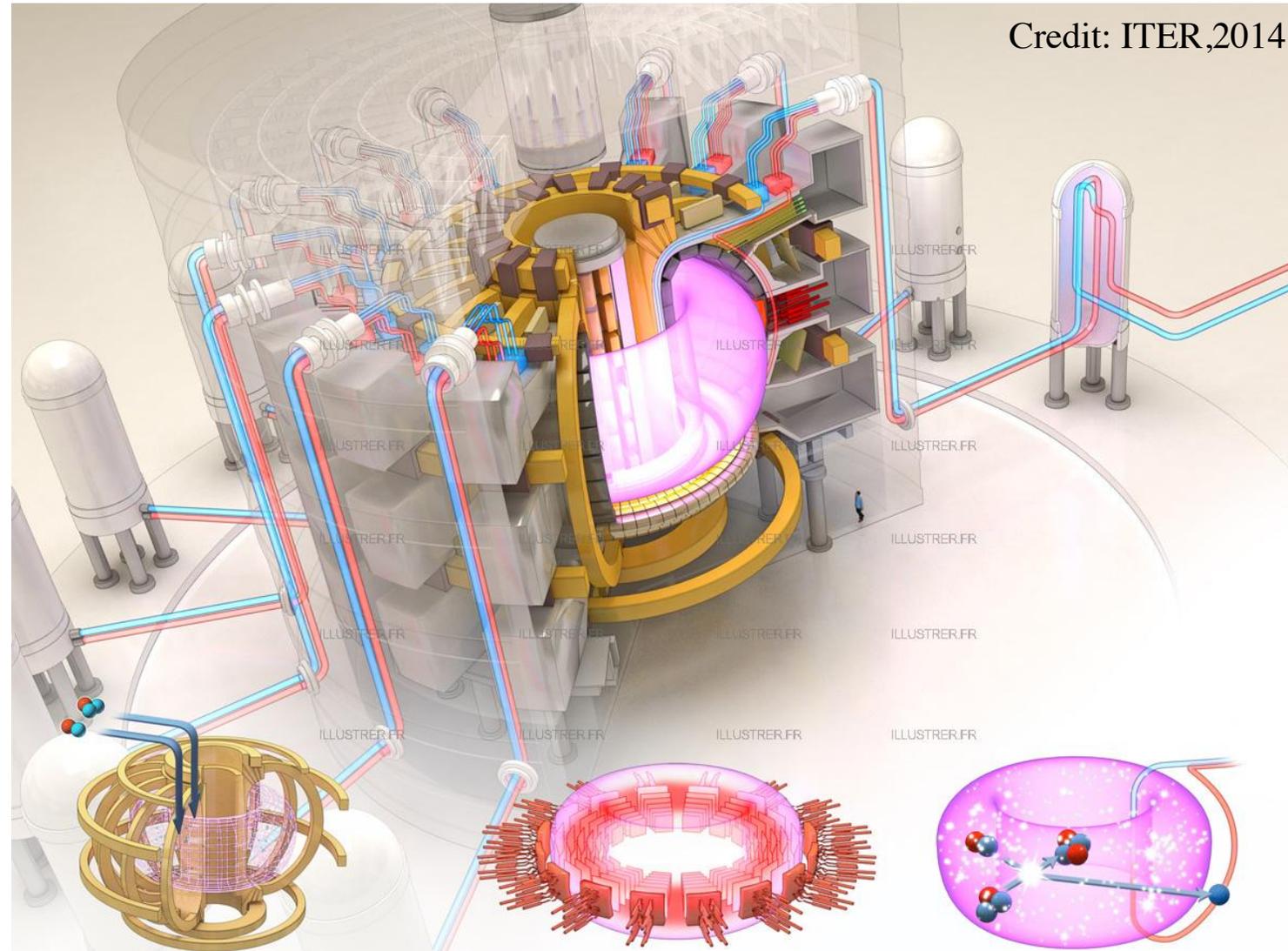
First demonstration of $^3\text{He}^3\text{He}$ reactions in a plasma in 2005



The ^3He on Earth is Insufficient to Support Fusion Power

There is <100 kg of available terrestrial ^3He

Only enough to operate a GWe fusion power plant for 1 year



The Moon has retained over 1 million tonnes of ^3He

Solar Wind

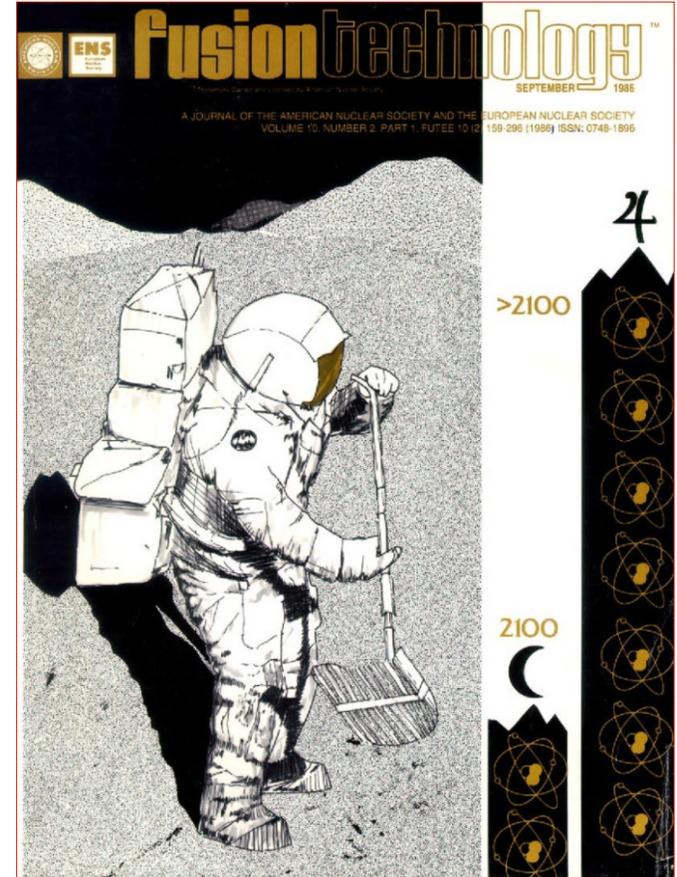
96% H^+

4% He^{++}

0.002% $^3\text{He}^{++}$



Total ^3He to hit the Moon
is about **500 million tonnes**
over 4.5 billion years



L.J. Wittenberg, J.F. Santarius, and G.L. Kulcinski, "Lunar Source of ^3He for Commercial Fusion Power," *Fusion Technology* **10**, 167 (1986).



^3He on the Moon Could Become Extremely Valuable

One of today's SpaceX Dragon capsules could return a "payload" of ^3He worth around \$15 billion in energy.

40 Tonnes (12 Dragon capsules) of ^3He Could Provide all the Electricity Used in North America in 2014

At today's oil prices (\$8.5/million BTU or \$50/barrel) the energy content in one tonne of ^3He would be worth \$4.4 billion



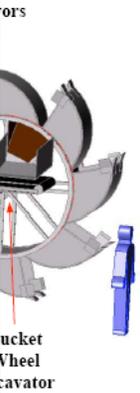
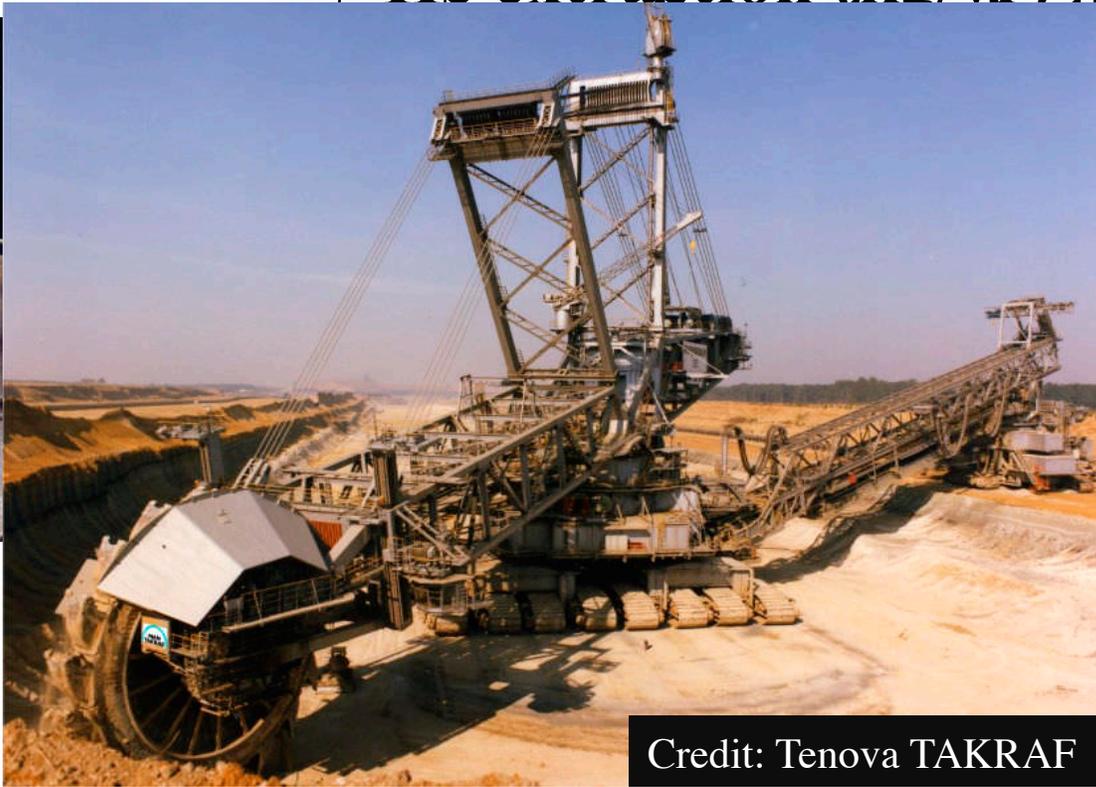
Credit: SpaceX, 2012



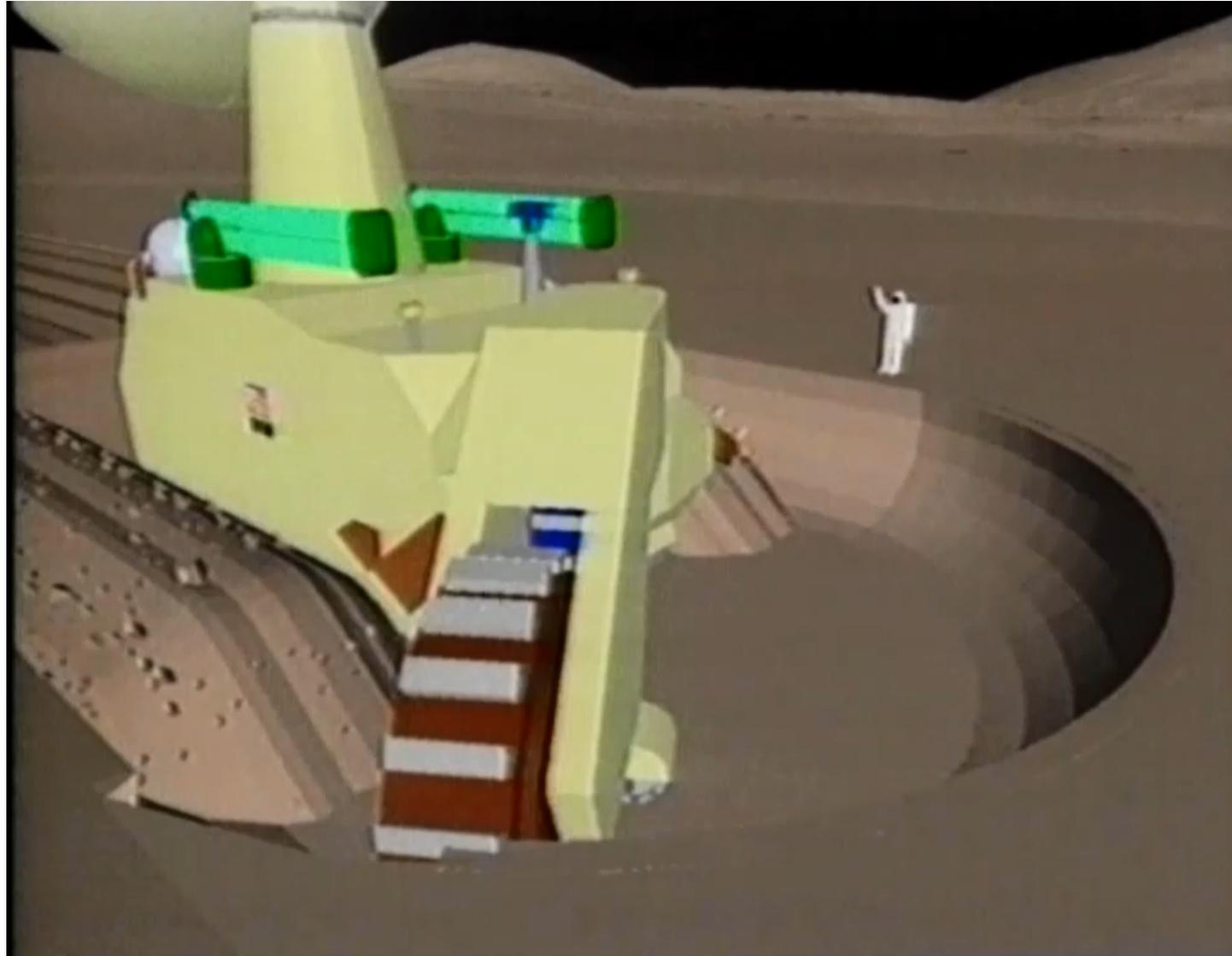
There are Three Wisconsin Lunar ^3He Miner Designs

Excavation rate (tonnes/hr)	1258
Processing rate (tonnes/hr)	5563
Thermal processing goal (tonnes/hr)	66
^3He extraction (kg/yr)	66

TAKRAF SR 8000 bucket-wheel excavator can excavate > 16,000 tonnes/hr of bituminous coal and has a mass of 14,200 tonnes



There are Four Main Processes in a ^3He Miner



**Excavate and
Convey**

Beneficiate

**Heat Regolith
and Evolve
Volatiles**

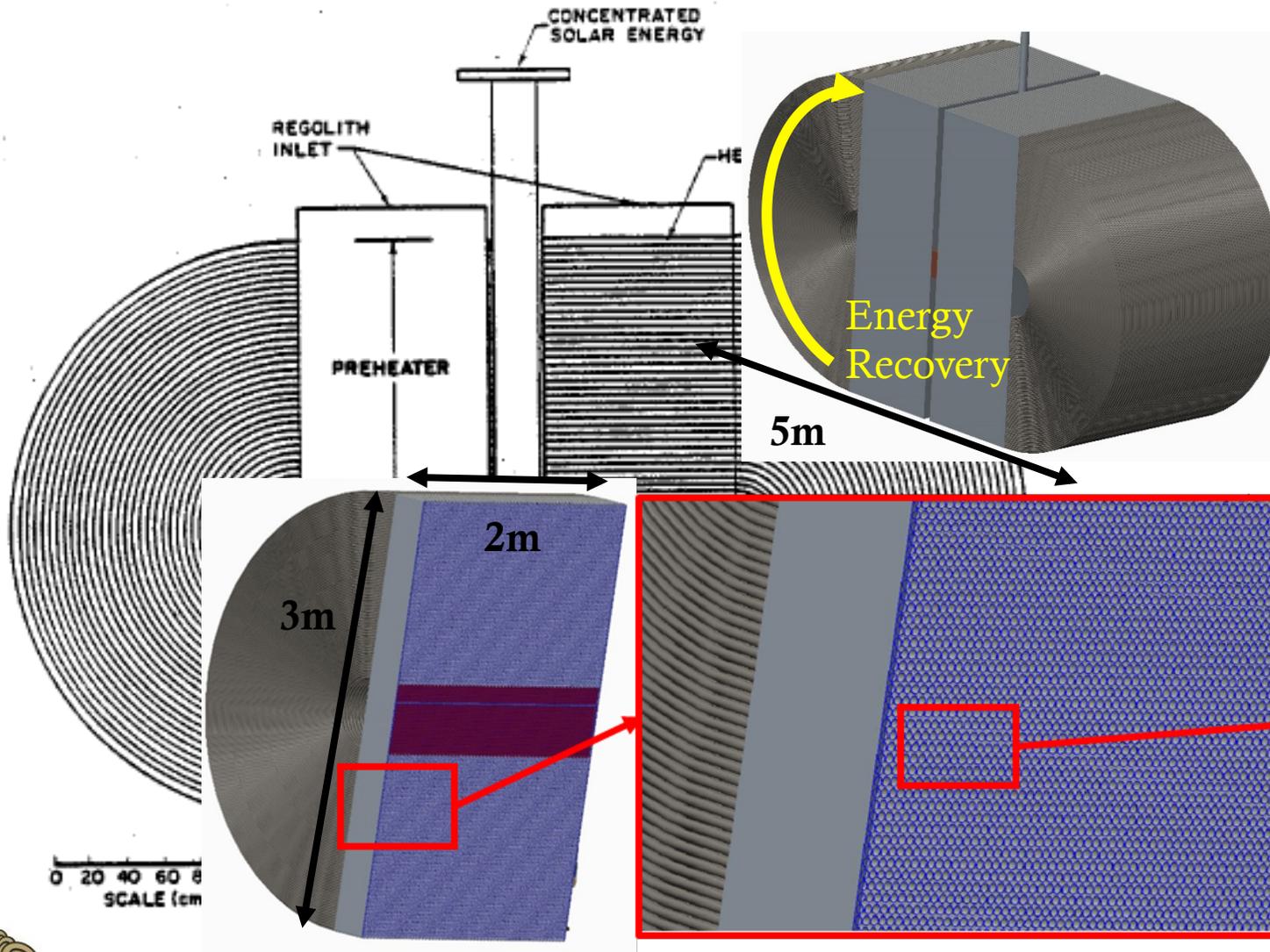
**Collect
Volatiles**

Credit: Bechtel, 1992





The Heat Pipe Heat Exchanger is the Key Part of the Miner



energy recovery by using heat pipes

17 MW from solar collector instead of 82 MW

157 kg/s of regolith from 30 °C up to 700 °C
 release 85% of embedded helium-3

produces 16.7 g/hr of ³He (66 kg in 3942 hours of operation)

combinations
 to ~250 °C
 operating
 stainless steel pipes:

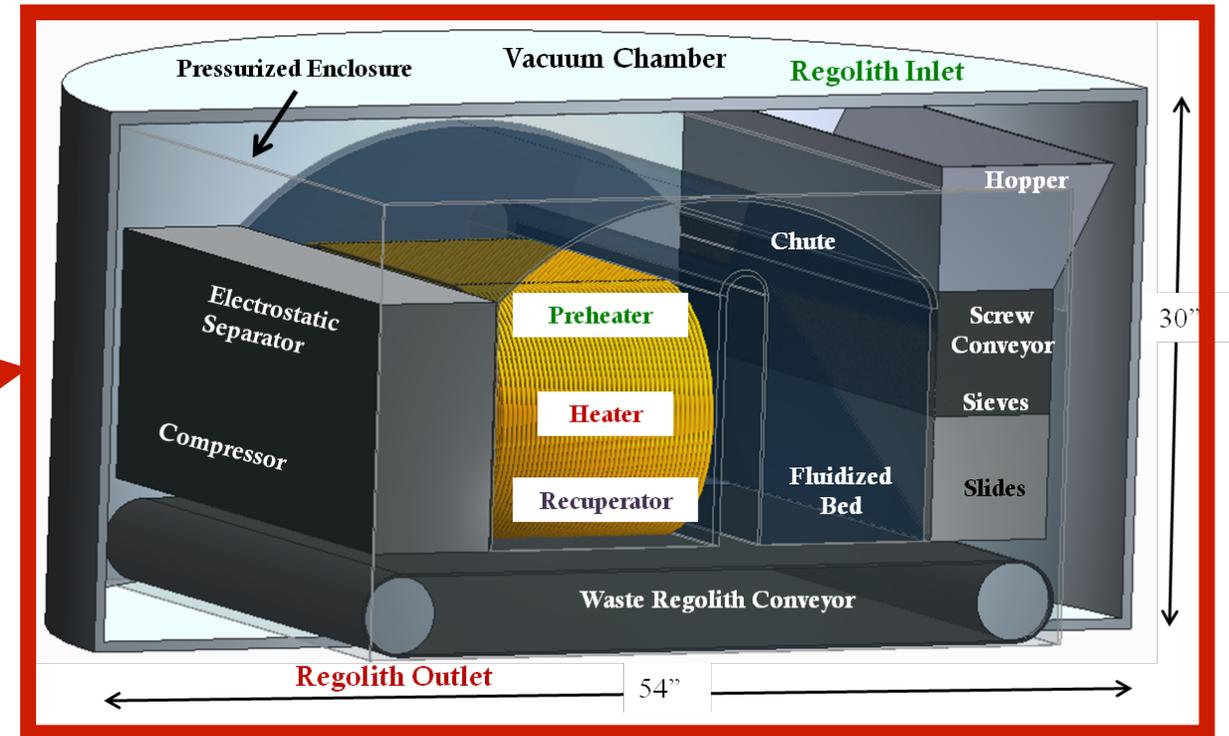
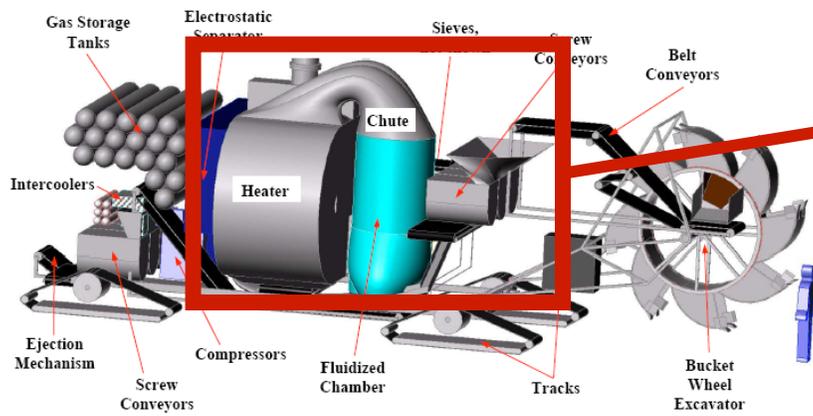


Research to Demonstrate the ^3He Miner Heating System

Main Research Question: How Effectively can ^3He be Extracted?

- First Demonstration of ^3He release inside of a heat pipe heat exchanger
- 1:1000 scale mass flow rate relative to M-3 (157 g/s)

Helium Extraction and Acquisition Test bed (HEAT)



There are Two Main Areas to this Research

Small Scale Demonstration of Lunar ^3He Extraction

- Implant He into Simulant
- 1kg Batches of Simulant
- Known Concentrations

Credit: M. Druckmüller

Helium Implantation

- Regolith Temperature to 700°C
- Heat Recovery Measurement
- He Release Measurement

Regolith Outlet

HEAT



JSC-1A Lunar Regolith Simulant Will be Used



Minerals	JSC-1A	on
Plagioclase	37.83	
Clinopyroxene	18.77	
Orthopyroxene	0.66	%
Olivine	12.44	e)
Glass	26.67	
Magnetite	0.01	
Chromite	0.00	
Ilmenite	0.11	
Sulphides	0.17	
Iron	0.00	
MgFeAl Silicate	3.06	
K Feldspar	0.07	
Quartz	0.01	
Calcite	0.11	
Others	0.07	
Total	100.00	

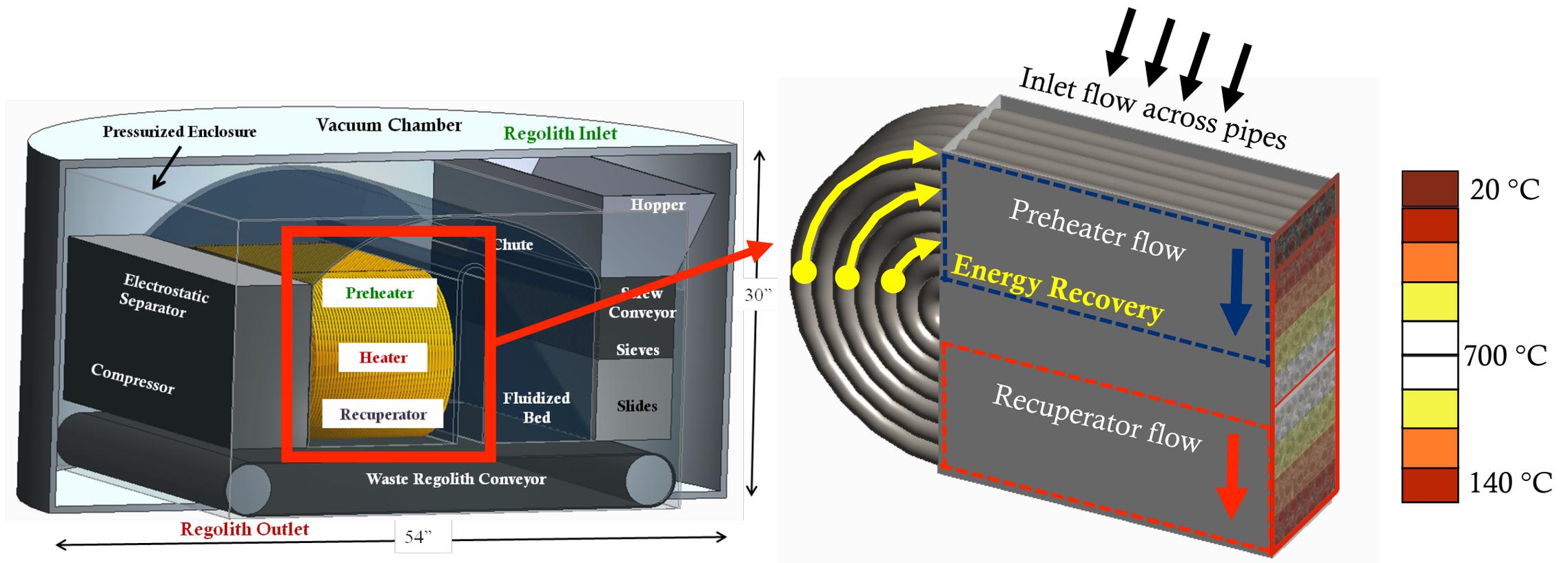
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Thanks to Dr. James Manton for 101 kg of JSC-1A from NASA/NSU

Specific heat	700- 1400 [J/kg-K]	1047.41 log(Temp) - 1848.15 [J/kg-K]
Thermal Conductivity @20 kPa	0.15 - 0.40 [W/m-K]	3.9e ⁻⁴ (Temp) + 0.1588 [W/m-K]
Cohesion	1 kPa	1 kPa
Angle of Internal Friction	40-55 degrees	45 degrees

JSC-1A Merriam Crater Cinders (left) and ground regolith simulant (right). Credit: ORBITEC

The Heat Pipe HX (HPHX) is the Key Part of HEAT



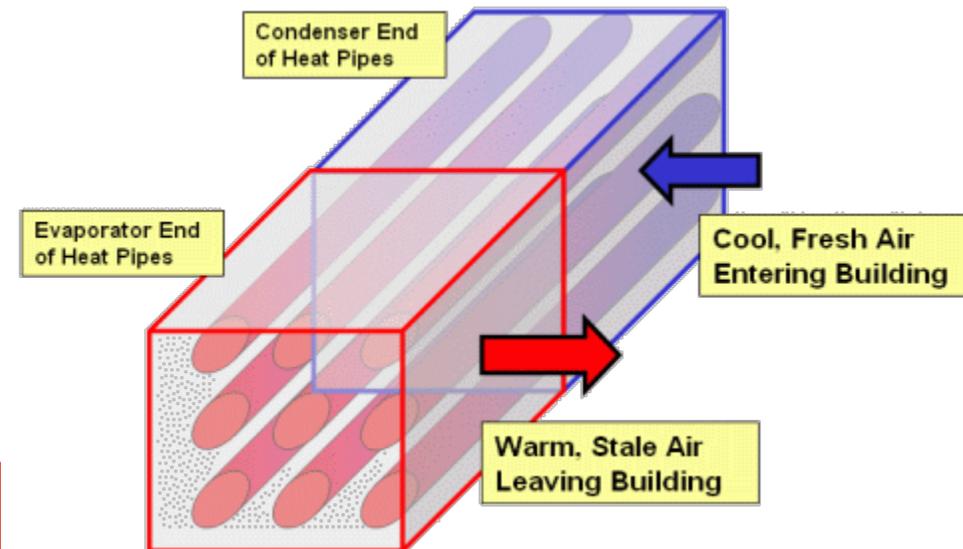
HPHX Design: Staged Counterflow HX Analysis

- Energy balance on cold and hot streams of regolith
- Effectiveness – NTU method
- Stage temp., effectiveness, conductance determined
- Stage change in regolith temperature determined
- HX surface area determined

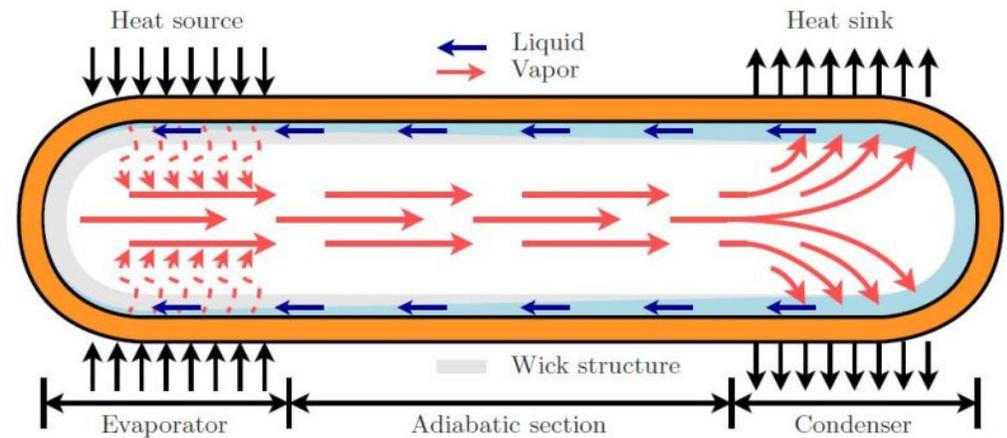
$$Q = C_h (T_{hi} - T_{ho}) = C_h \epsilon (T_{hi} - T_p) = C_c (T_{co} - T_{ci}) = C_c \epsilon_c (T_p - T_{ci})$$

$$\epsilon_h = \frac{T_{hi} - T_{ho}}{T_{hi} - T_p} = 1 - e^{-NTU_h} \quad \epsilon_c = \frac{T_{co} - T_{ci}}{T_p - T_{ci}} = 1 - e^{-NTU_c}$$

$$NTU_h = \frac{h_h A_h}{C_h} \quad NTU_c = \frac{h_c A_c}{C_c}$$

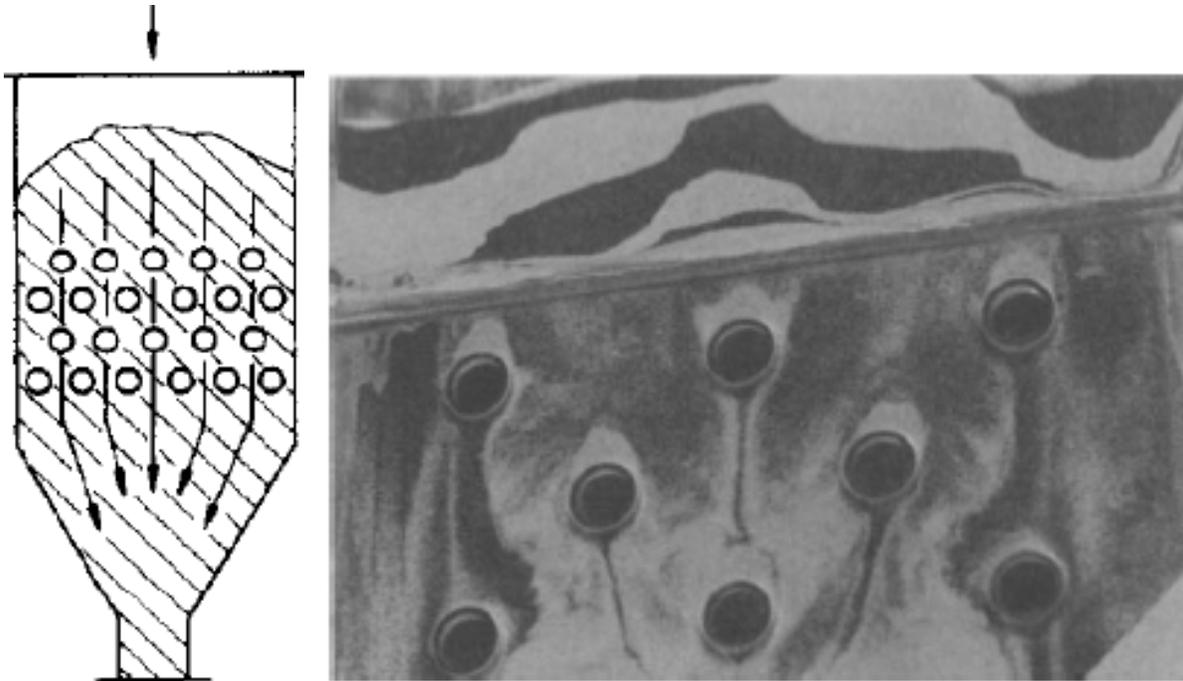


Credit: Des Champs Labs, 1993

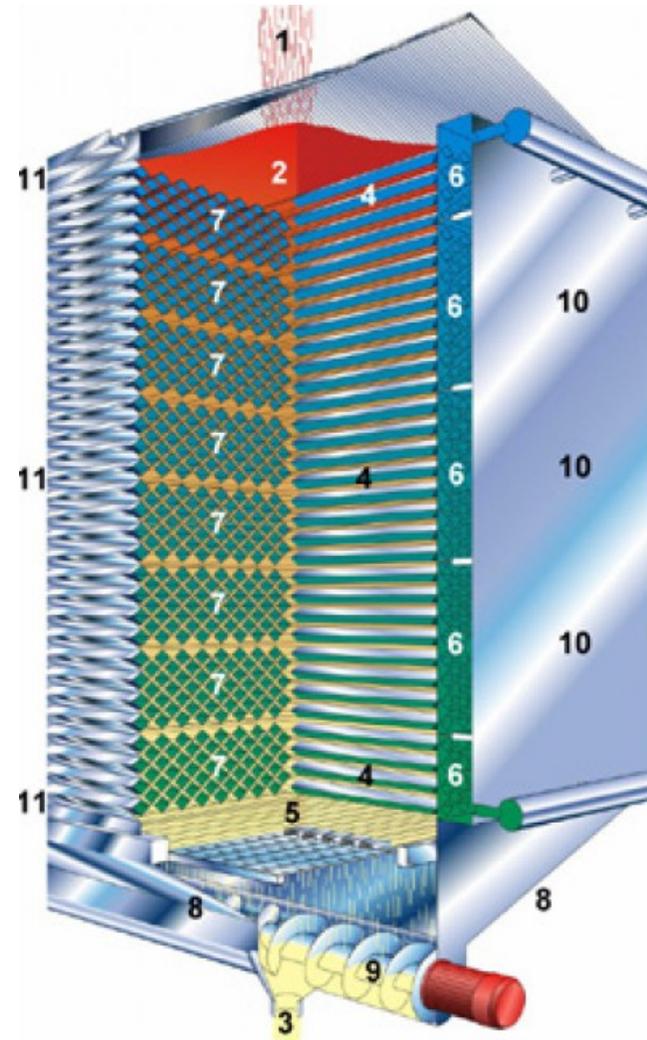


HPHX Design: Moving Bed Flow and Heat Transfer

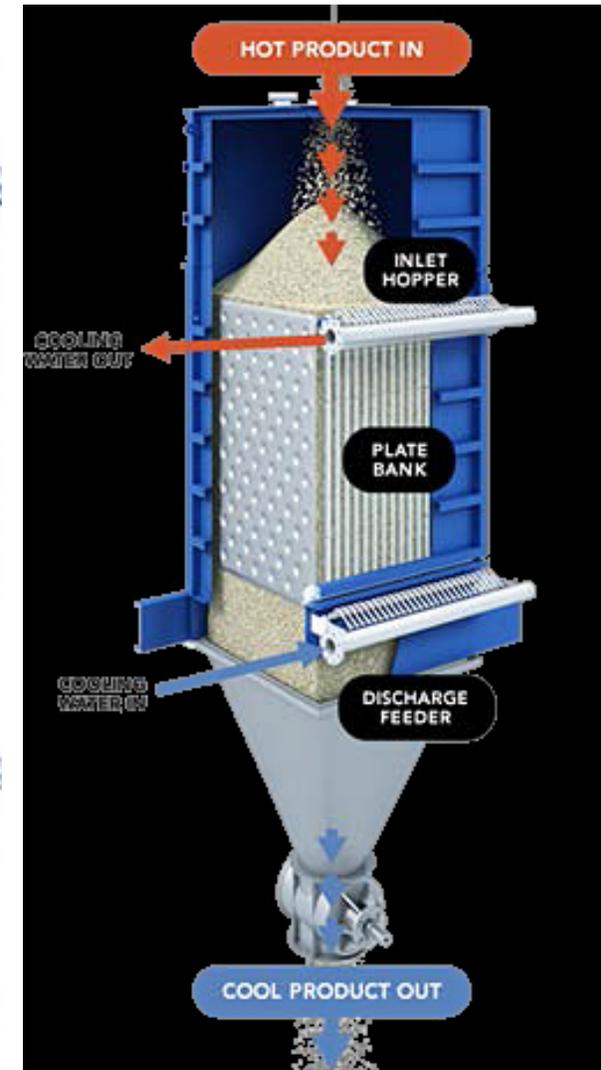
- Moving Bed Heat Exchangers
 - Thermal Energy Storage
 - Heat recovery from bulk solids



Credit: Niegsch et al., 1994



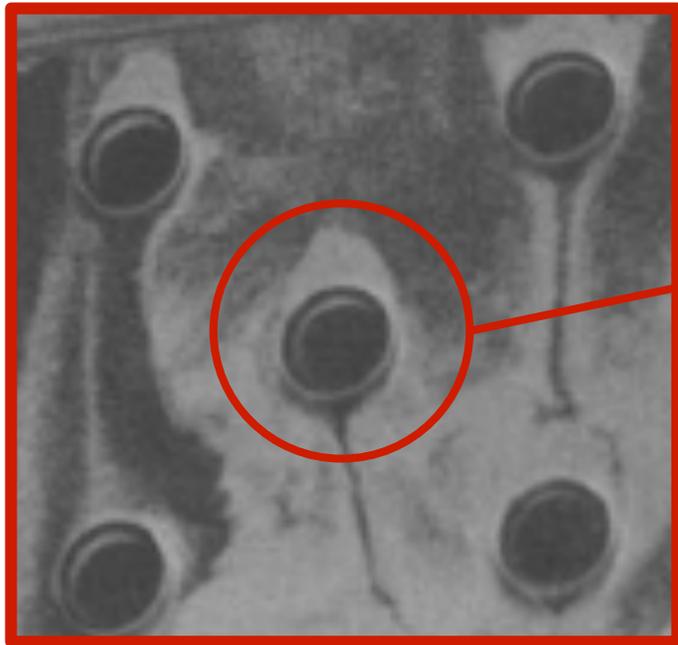
Credit: Grenzebach Group



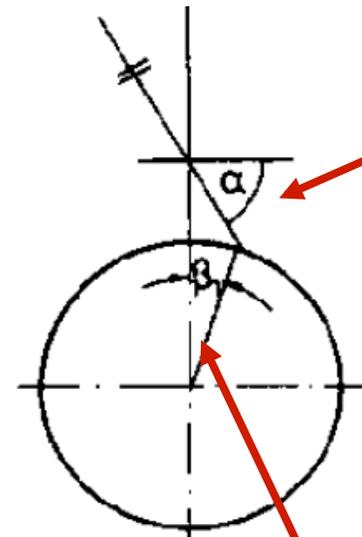
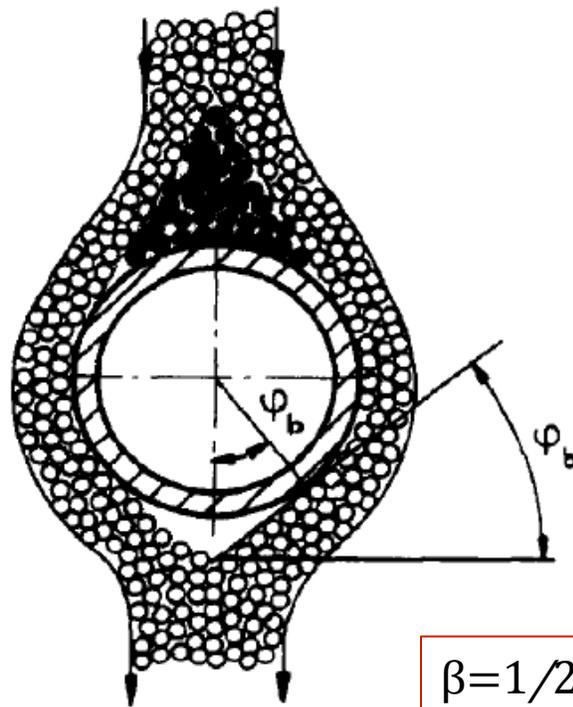
Credit: NETL/DOE, 2014

HPHX Design: Moving Bed Flow Model

- The granular friction properties influence the flow channel shape
- The Niegisch model (Niegisch et al., 1994) incorporates the stagnation and void areas of flow



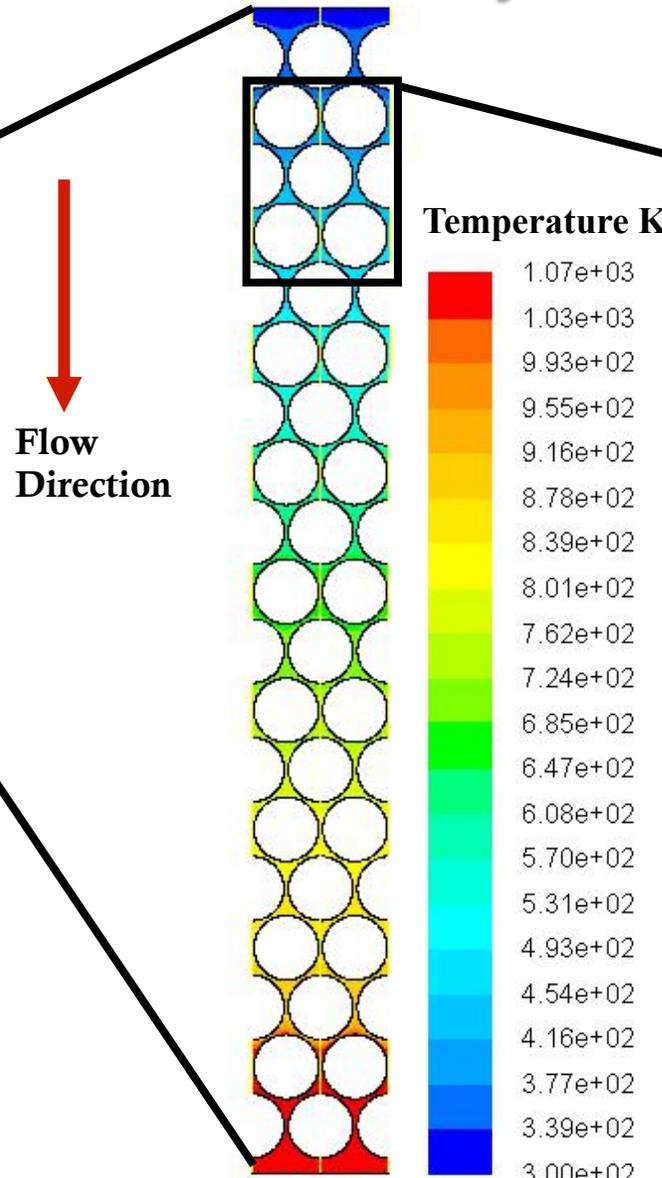
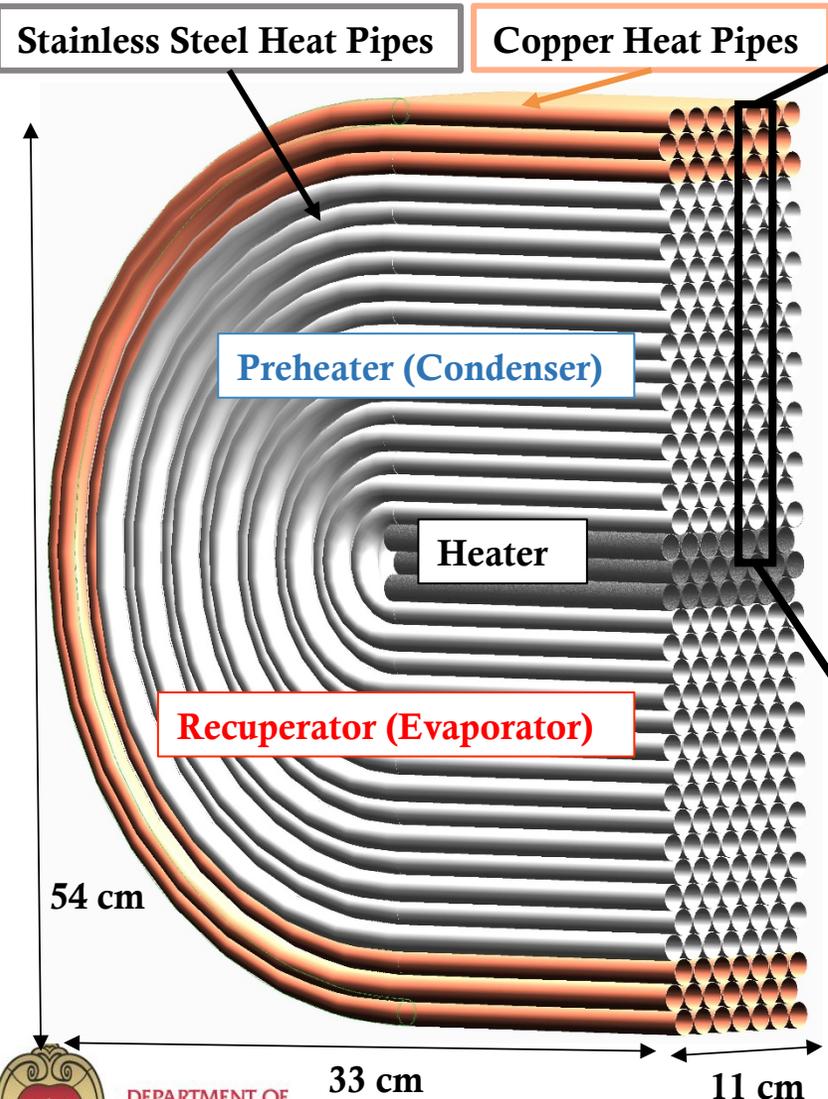
Credit: Niegisch et al., 1994



$$\alpha = \pi/4 + \varphi \downarrow e$$

$$\beta = 1/2 [\cos \uparrow - 1 (1 - \sin(\varphi \downarrow e) / 2 \sin(\varphi \downarrow e)) + \sin \uparrow - 1 (\sin(\varphi \downarrow w) / \sin(\varphi \downarrow e)) + \varphi \downarrow w]$$

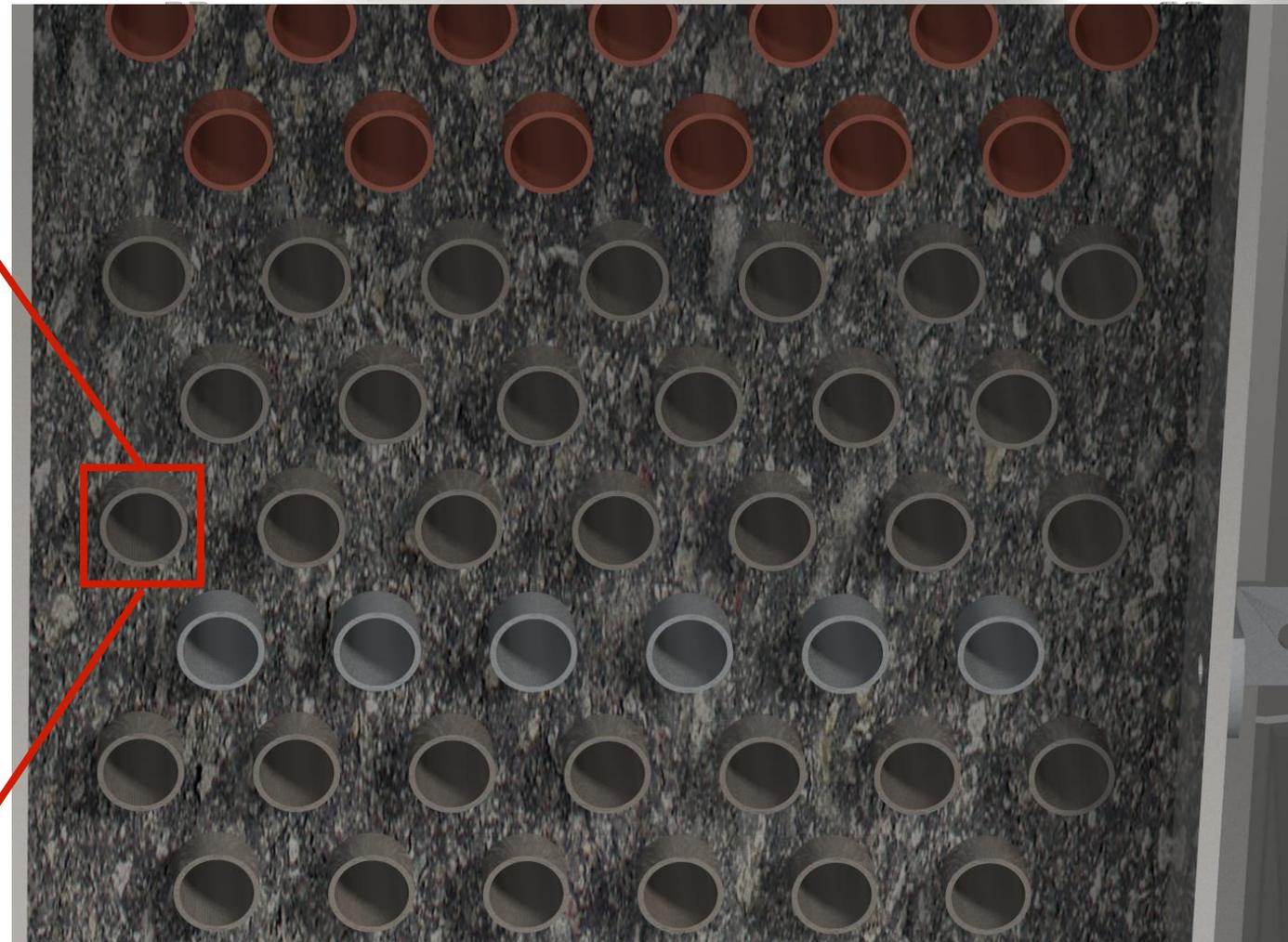
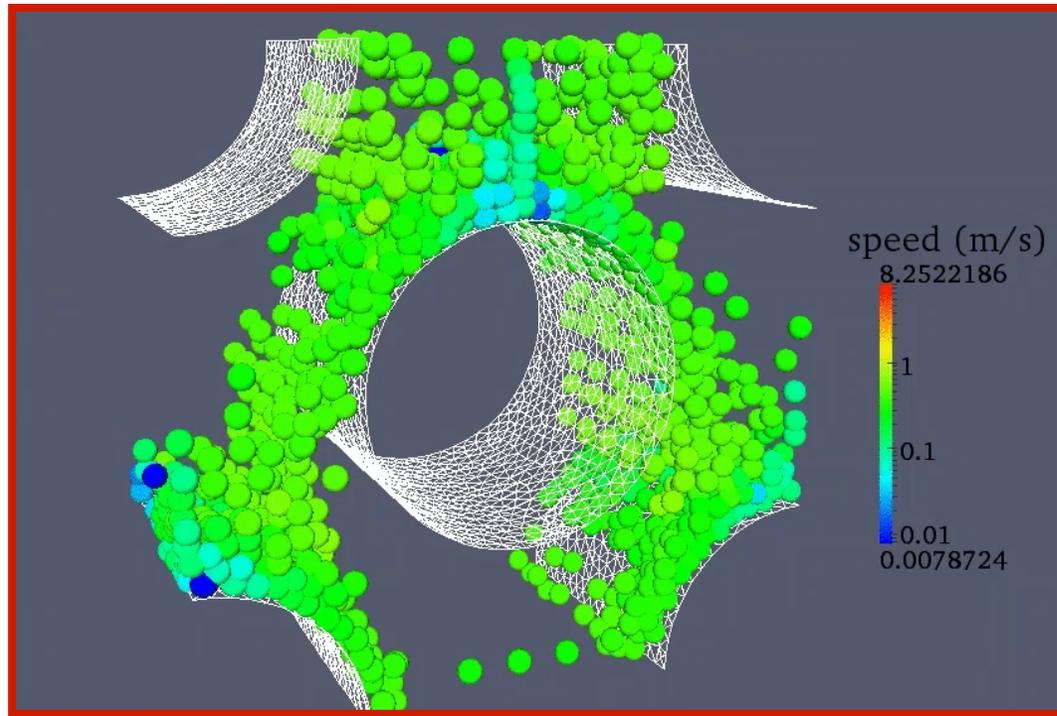
HPHX Design: Preliminary Thesis Design Work



Heat pipes	119
Columns	7
Rows	17
Pipe outer diameter	1.5 cm
Pipe heat exchanging length	22.3 cm
Heater rows	3
Distance between pipe columns	1 mm
Heat exchanger mass	6 kg
Heat exchanger height	54 cm
Heat exchanger width	10.7 cm

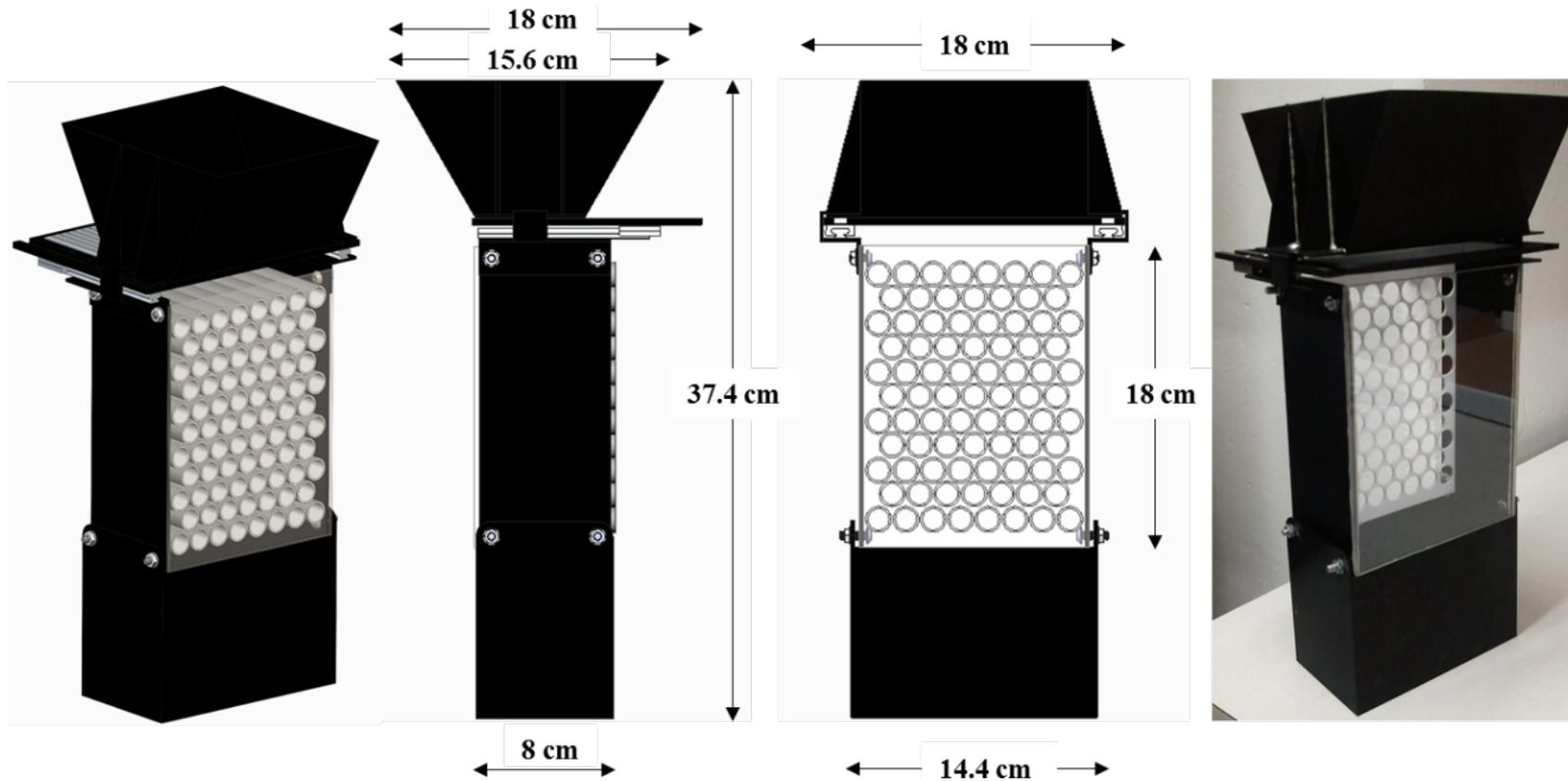
Verify HPHX Design: Testing of Flow and Heat Transfer

- Pipe to Regolith Heat Transfer Coefficient
- Minimum pipe spacing
- Verification of Analysis



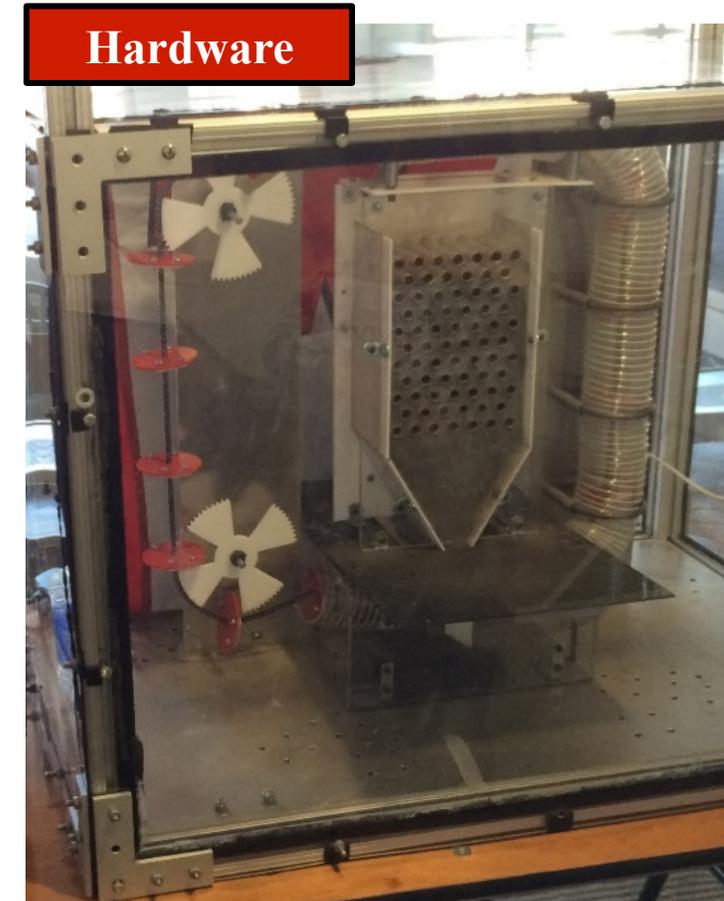
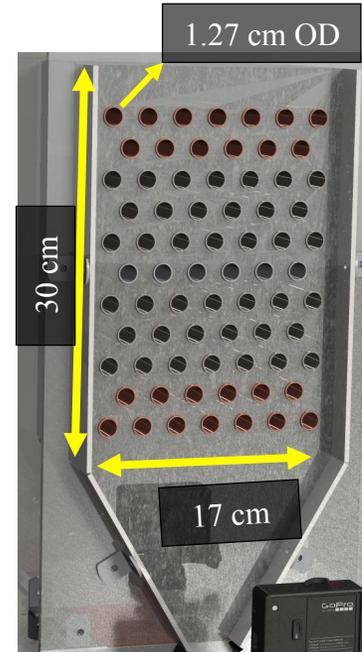
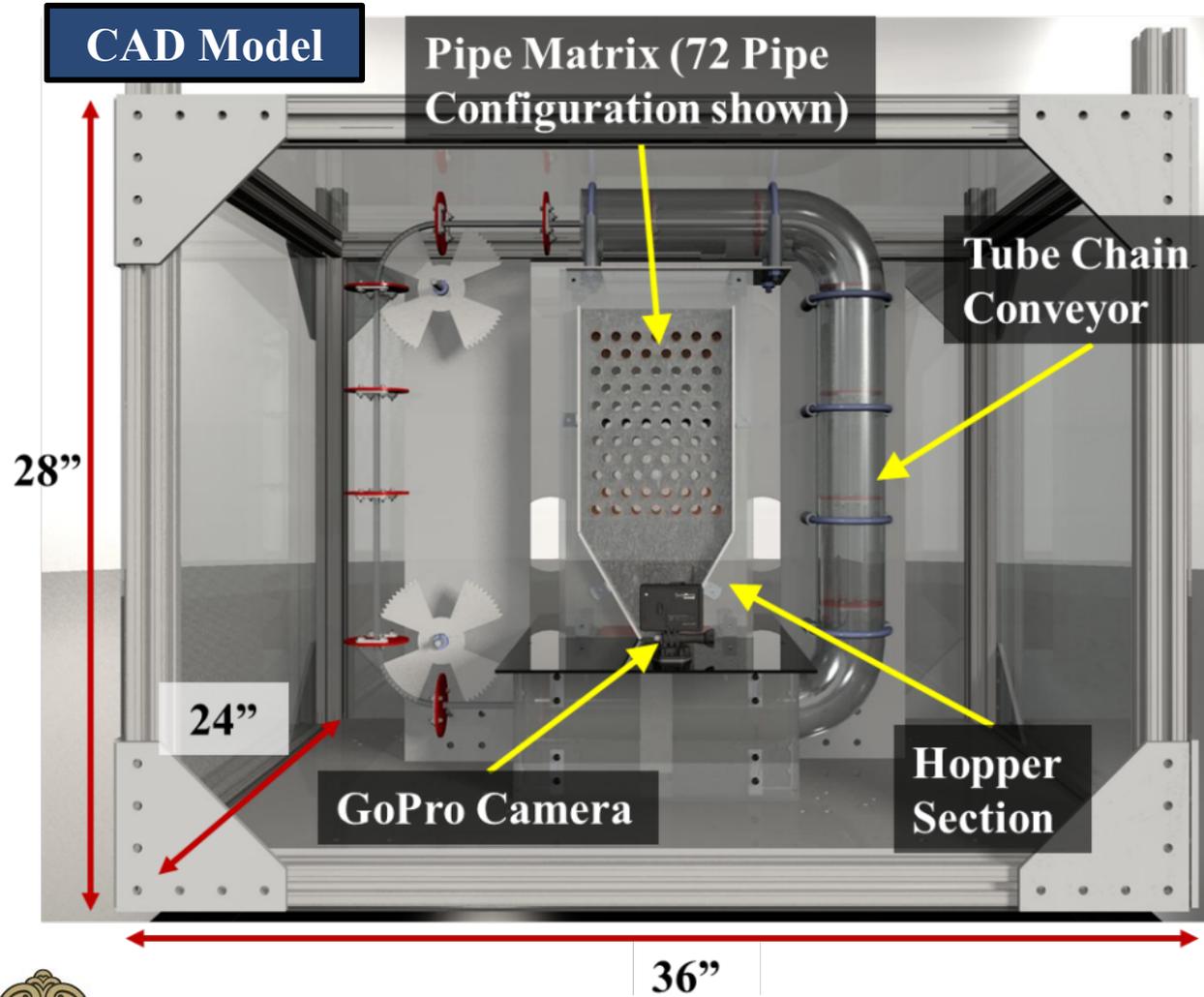
Verify HPHX Design: Granular Flow Experiment (GFX)

- The first iteration of testing allowed for a better second iteration
- Particle Image Velocimetry (PIV) to be used as with other studies



Credit: Olson, Strange, Atruksang

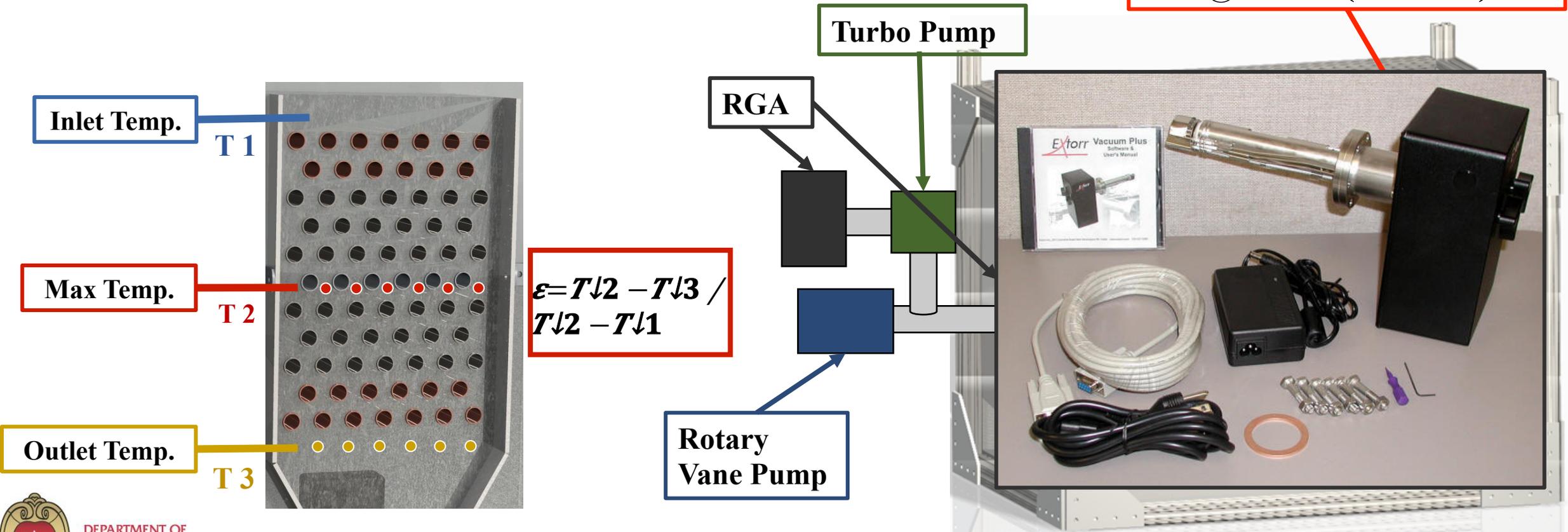
Verify HPHX Design: GFX V.2 Nearly Complete



Build and Test HPHX : High Temp, Instrumentation, Procedure

- RGA to be implemented to be calibrated for high temp at steady state (900°C)
- Flow rate of gas measured (with coupler, Pyrometer 2 seconds)
- Residual gas temperature and RGA measurements chamber

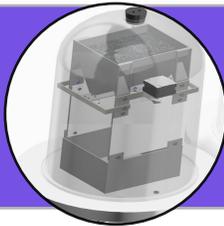
Interior Atmosphere: Argon
@20 kPa (150 Torr)



There are Two Aspects to Implantation into JSC-1A

- Implantation energy: 1 keV/amu
- Aim for 20 ppb concentration
- ^4He diffuses out of regolith like ^3He (use ^4He for cost)

Implant ^4He

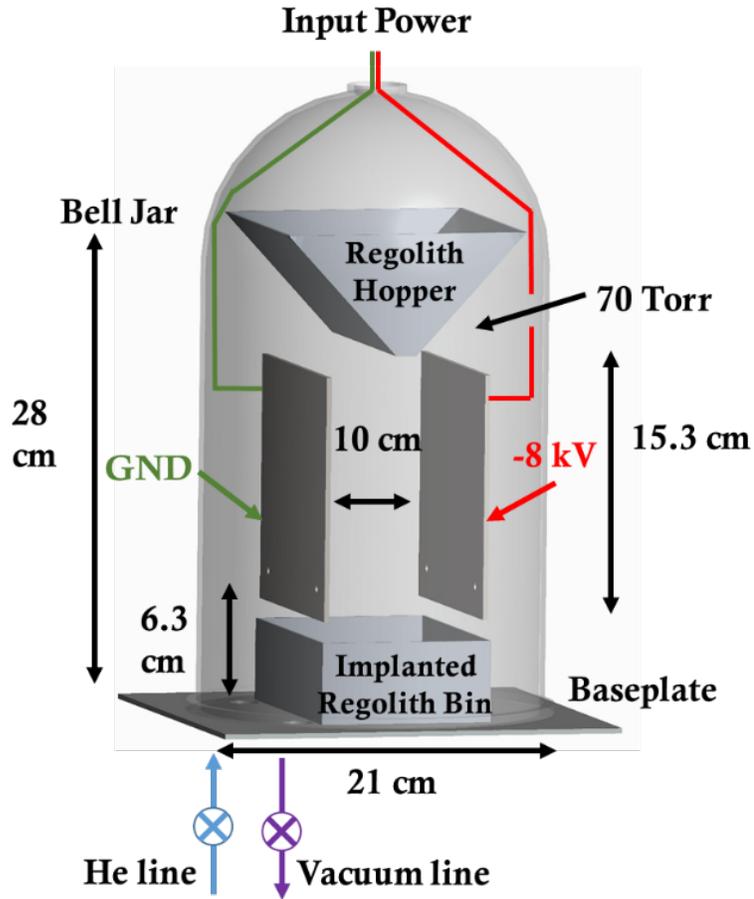


- Heat several ~1 g samples from ~1 kg batches to 1000°C
- Vacuum tube furnace, RGA
- Background ^4He concentration

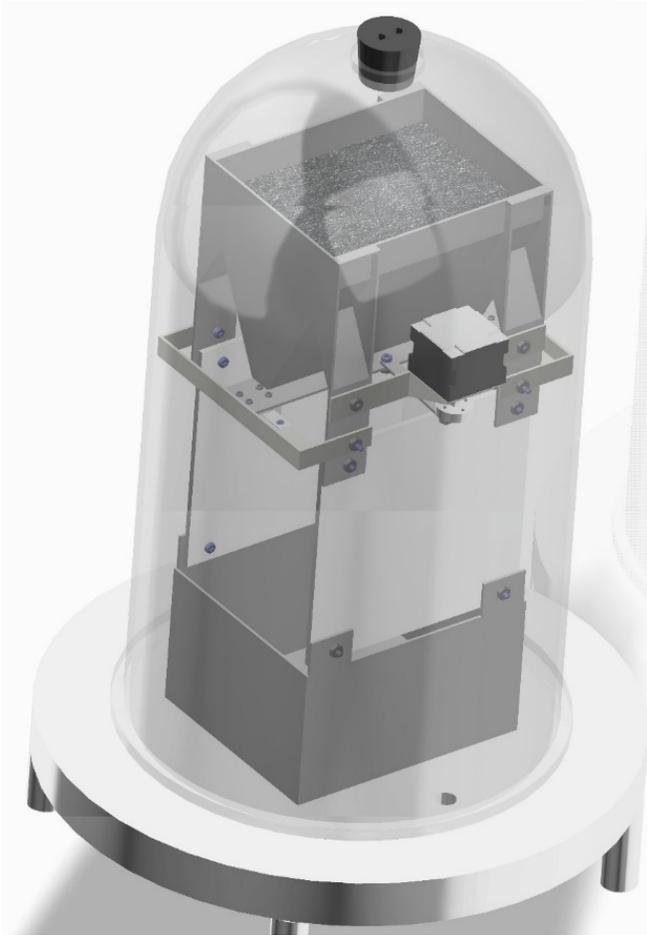
Measure Concentration



Implant Helium: From Concept to Construction



Concept: DC Plasma Discharge



Preliminary DC Plasma Discharge Design



KSC Swampworks Lab Dust Tolerant Vacuum Chamber



Conclusion

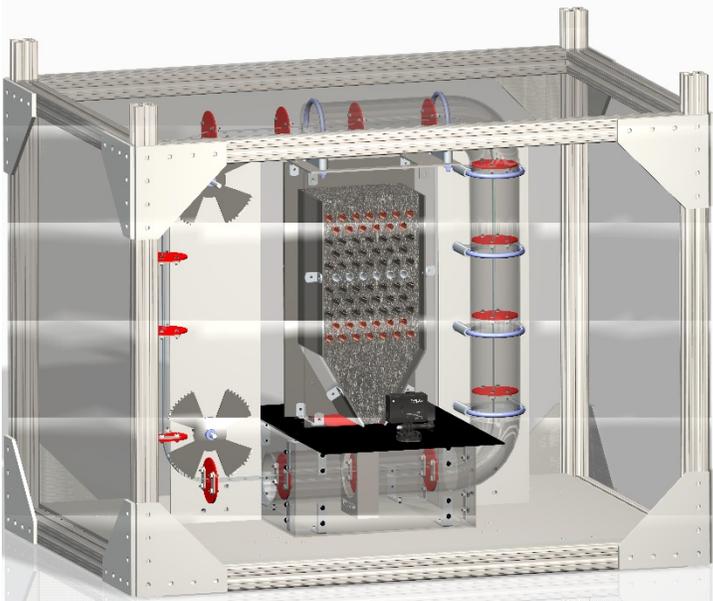
- First Demonstration of ^3He release inside of a heat pipe heat exchanger
- Requires development of HEAT and an Implantation device

Goal	Evaluation Criteria
^3He release rate of 5 $\mu\text{g/s}$ (1/1000 th of Mark series designs)	RGA measurements of atmosphere inside of the HEAT system
Achieve 85% thermal energy recovery efficiency	Change in temperature of the regolith simulant throughout the HEAT system as measured by thermocouples
Recommendations to improve the system for a future lunar pilot scale miner	Design alterations to increase the ^3He release rate and the energy recovery efficiency

Wisconsin ^3He Extraction Research Roadmap

Lab Prototypes

- Heating System Optimization
- Evolved ^3He Measurement



(UW HEAT GFX)

Lunar Gravity Testing

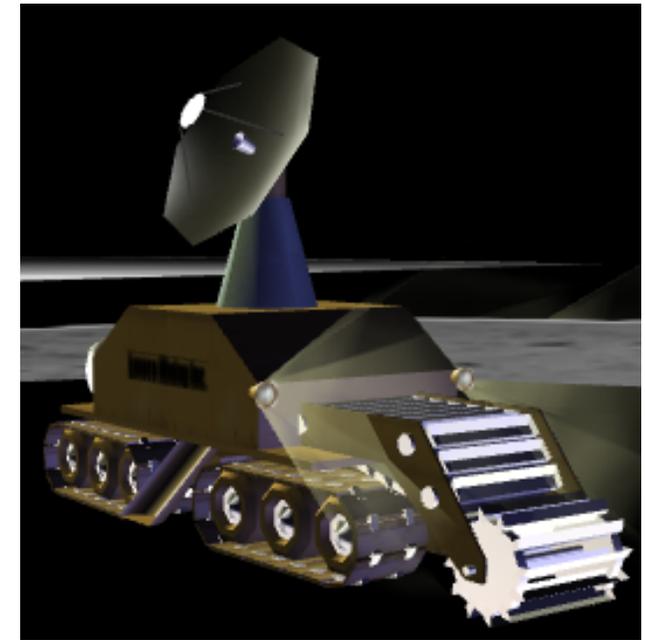
- Regolith Flow through Heating System in Lunar Gravity



(Lunar G HEAT)

Small Scale Lunar Mission

- INTERLUNE 1 Concept
- Use of GLXP Provider(s)?



(Micro ^3He Miner)



A Potential Roadmap for Lunar Helium-3

Prospecting and Research ~2015-2025

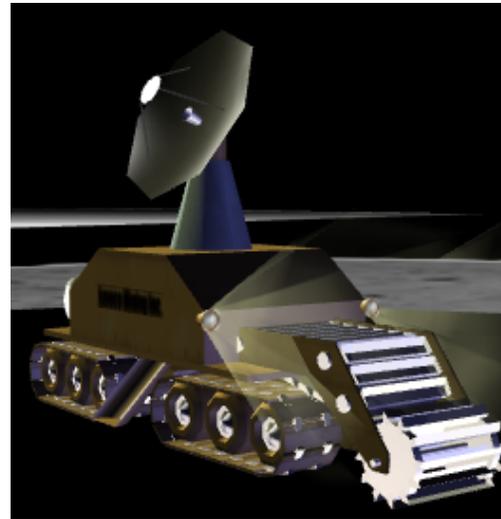
- Government missions
- **Research at UW-Madison**
- Google Lunar X-Prize



(NASA RESOLVE)

Small Scale Mining ~2025-2035

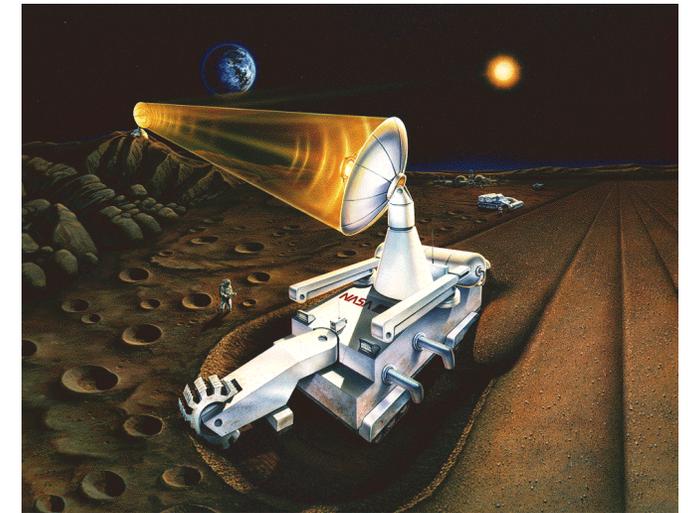
- First small test lunar miners
- Start of lunar outposts
- Other mining activities starting



(Small scale concept)

Established Mining Industry ~Post 2035

- Large lunar miners
- Established Moon-Earth shipping
- **^3He Fusion Reactors**



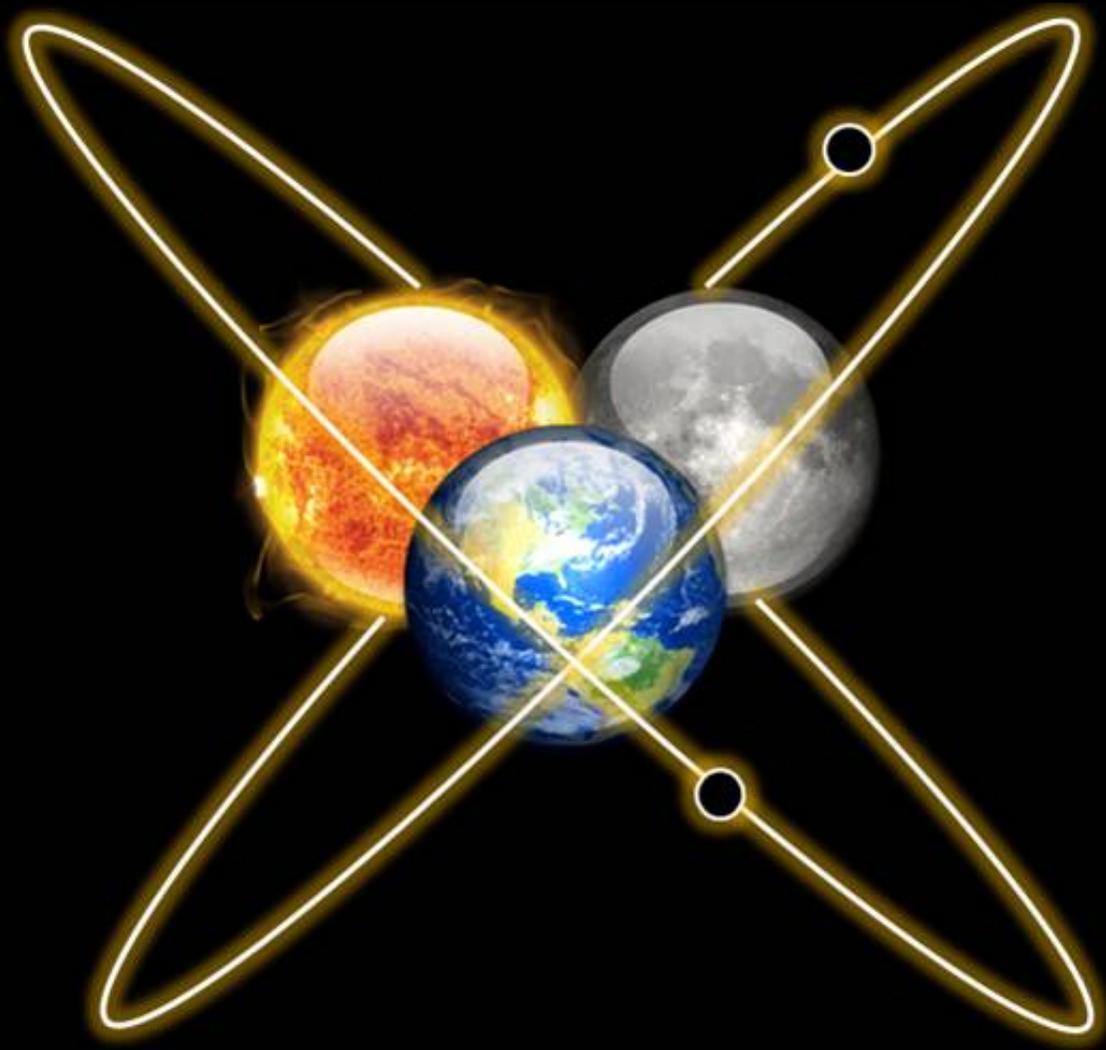
(UW Mark-II concept)



Questions?

Acknowledgments

- NASA Space Technology Research Fellowship Program
- Greatbatch Foundation
- Grainger Foundation
- Wisconsin Space Grant Consortium

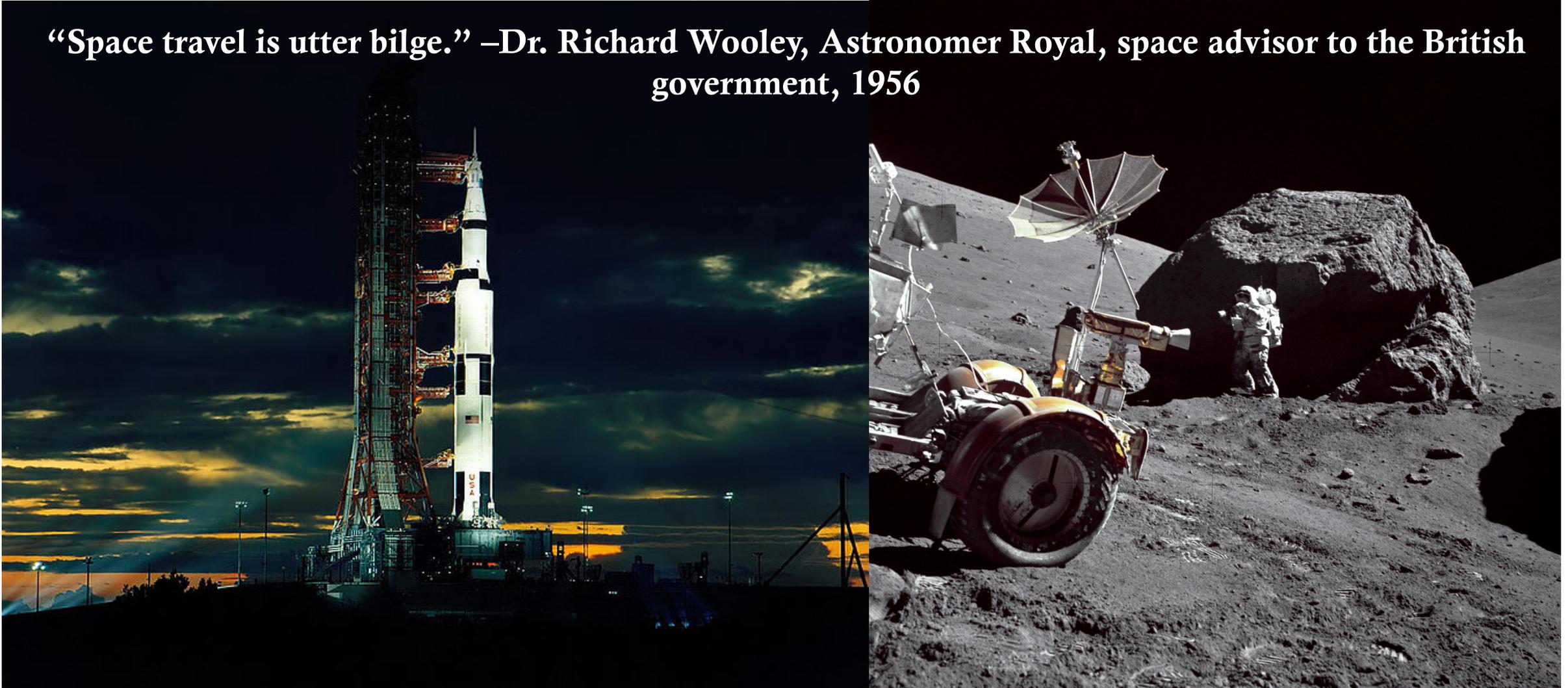


LUNAR HELIUM-3

THE EARTH'S ENERGY FUTURE

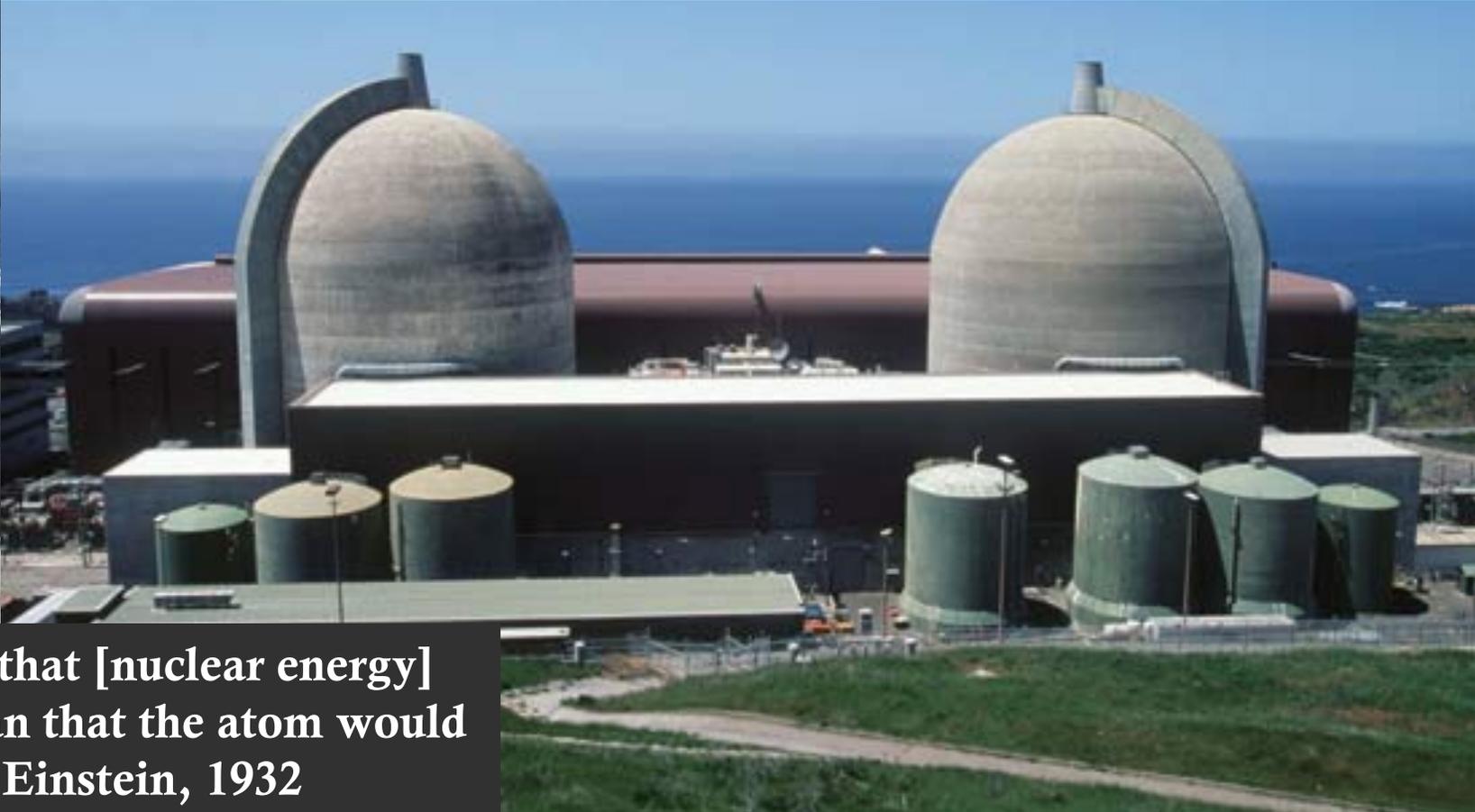
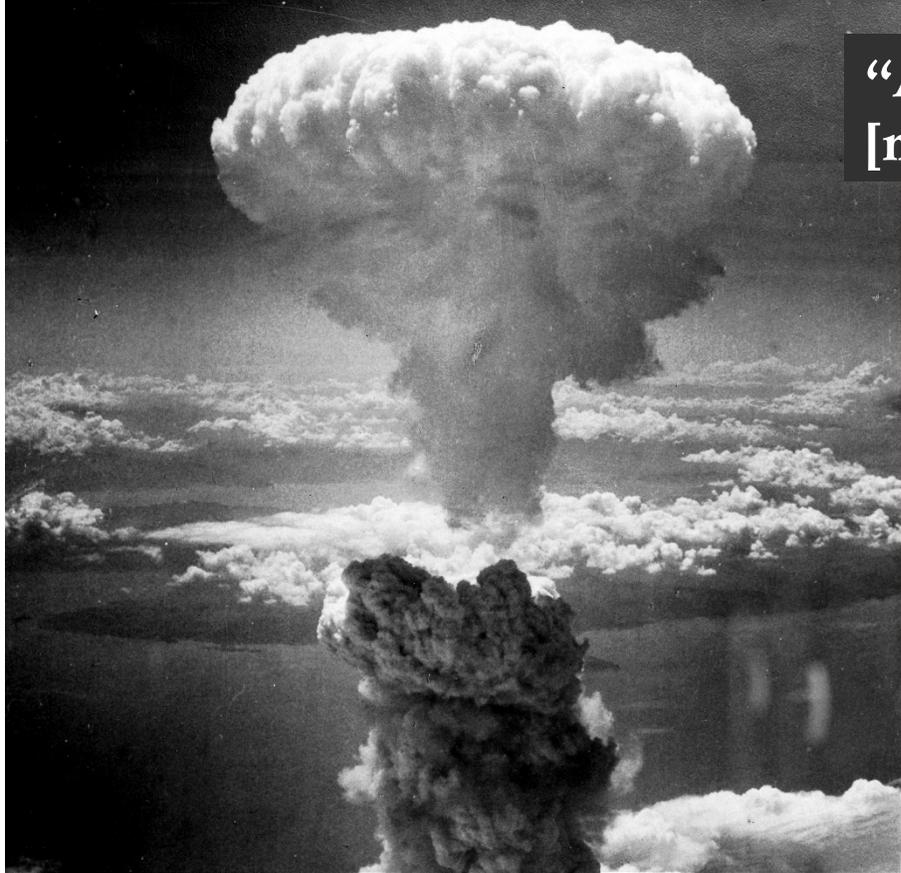
Mining ^3He and using it for Fusion Could Happen Sooner than you Think

“Space travel is utter bilge.” –Dr. Richard Wooley, Astronomer Royal, space advisor to the British government, 1956



Mining ^3He and using it for Fusion Could Happen Sooner than you Think

“Anyone who looks for a source of power in the transformation of the [nuclear of the] atom is talking moonshine.” –Ernest Rutherford, 1933



“There is not the slightest indication that [nuclear energy] will ever be obtainable. It would mean that the atom would have to be shattered at will.” –Albert Einstein, 1932

Upcoming Lunar ^3He Fusion Book

Lunar Helium-3 Fusion: The Earth's Energy Future

Follow-on to *Return to the Moon* by Dr. Harrison Schmitt, to be published in 2015

Discusses

- Increasing need for power worldwide
- Potential role of ^3He fusion technology
- Lunar bases and resources
- Legal regimes for lunar mining
- Economics of ^3He procurement
- Terrestrial fusion power plants
- Space applications of ^3He fusion
- Current lunar initiatives around the world



Authors: Dr. Harrison Schmitt, Dr. Gerald Kulcinski,
Dr. John Santarius, Aaron Olson

A.D.S. Olson CIM/PTMSS 5/13/2015

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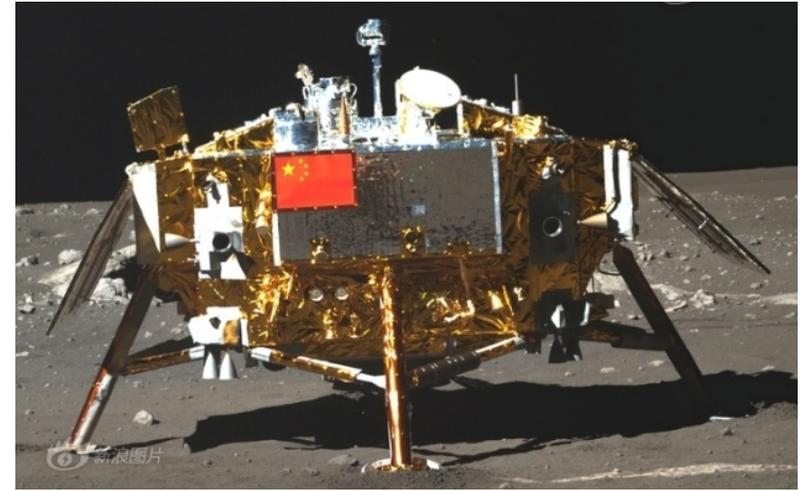
Lunar Mining and Prospecting Systems are Being Developed



Credit: Lockheed Martin, 2010



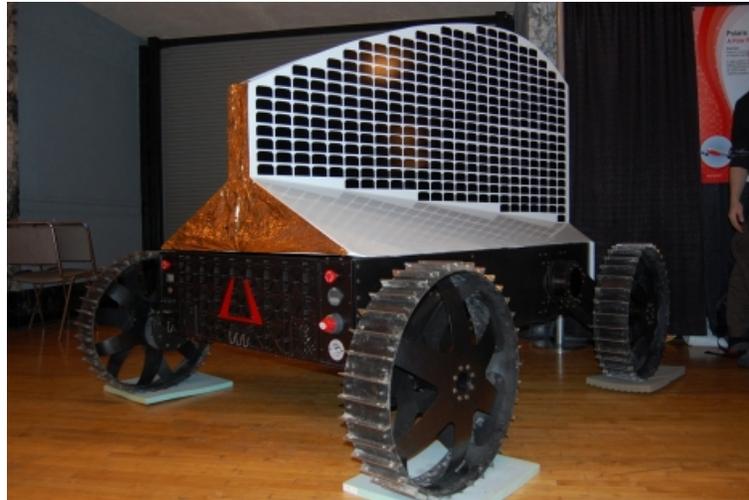
Credit: NASA KSC, 2012



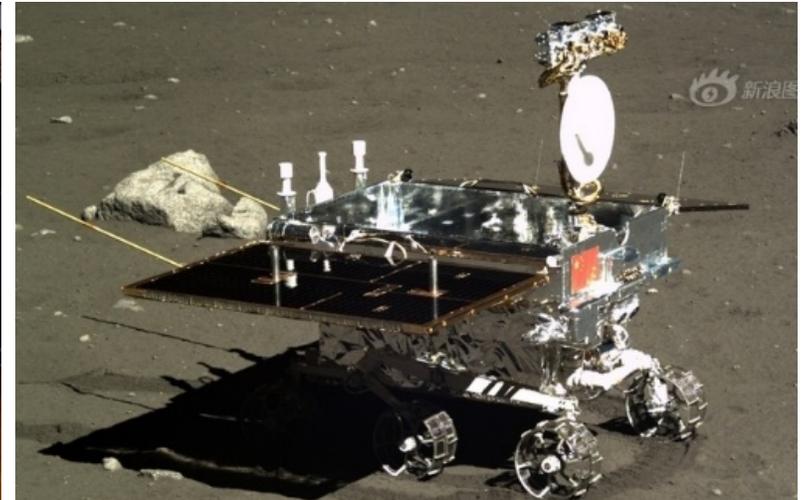
Credit: CNSA/CLEP, 2013



Credit: Laurentian U., 2011



Credit: Astrobotic, 2013



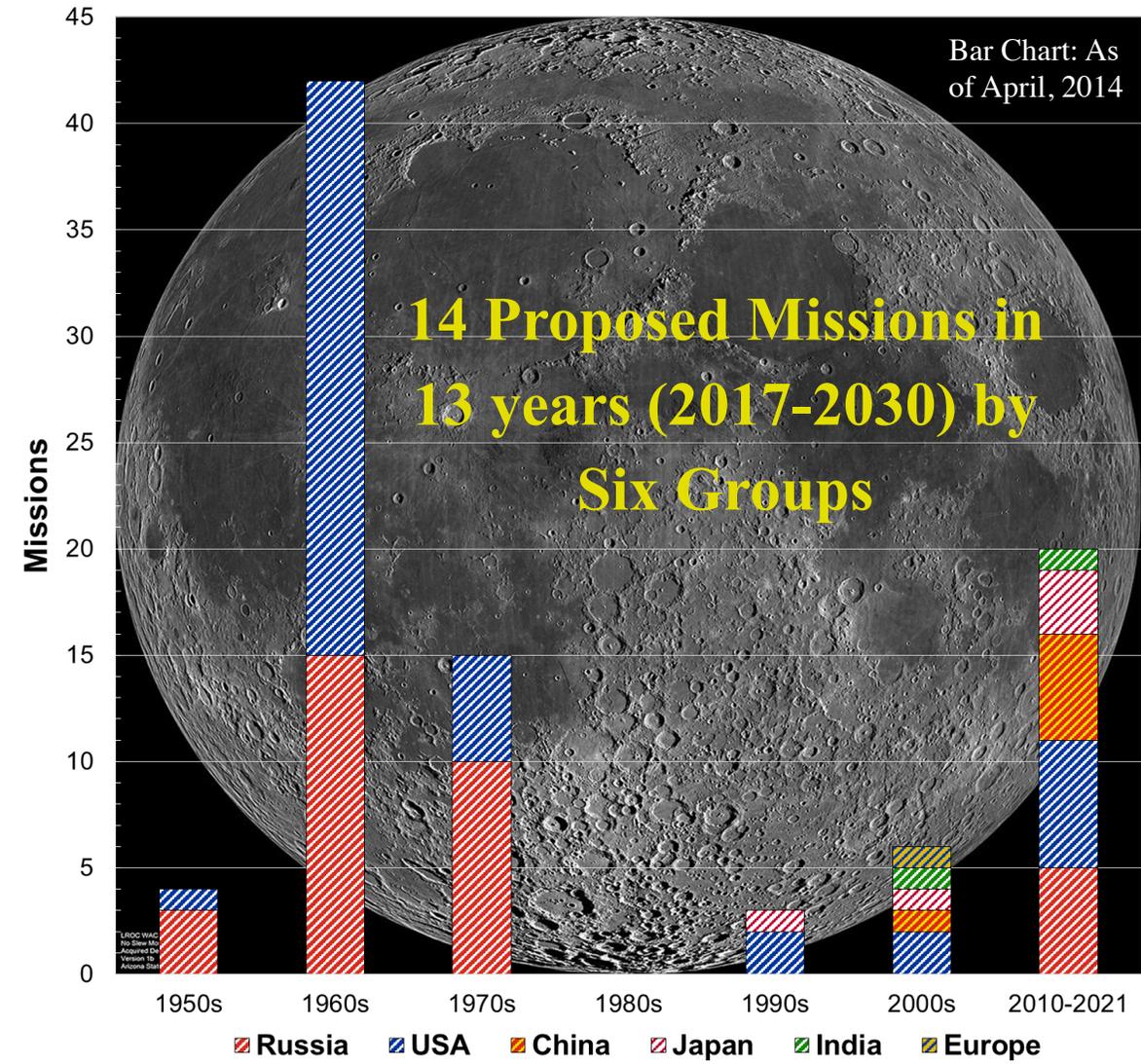
Credit: CNSA/CLEP, 2013



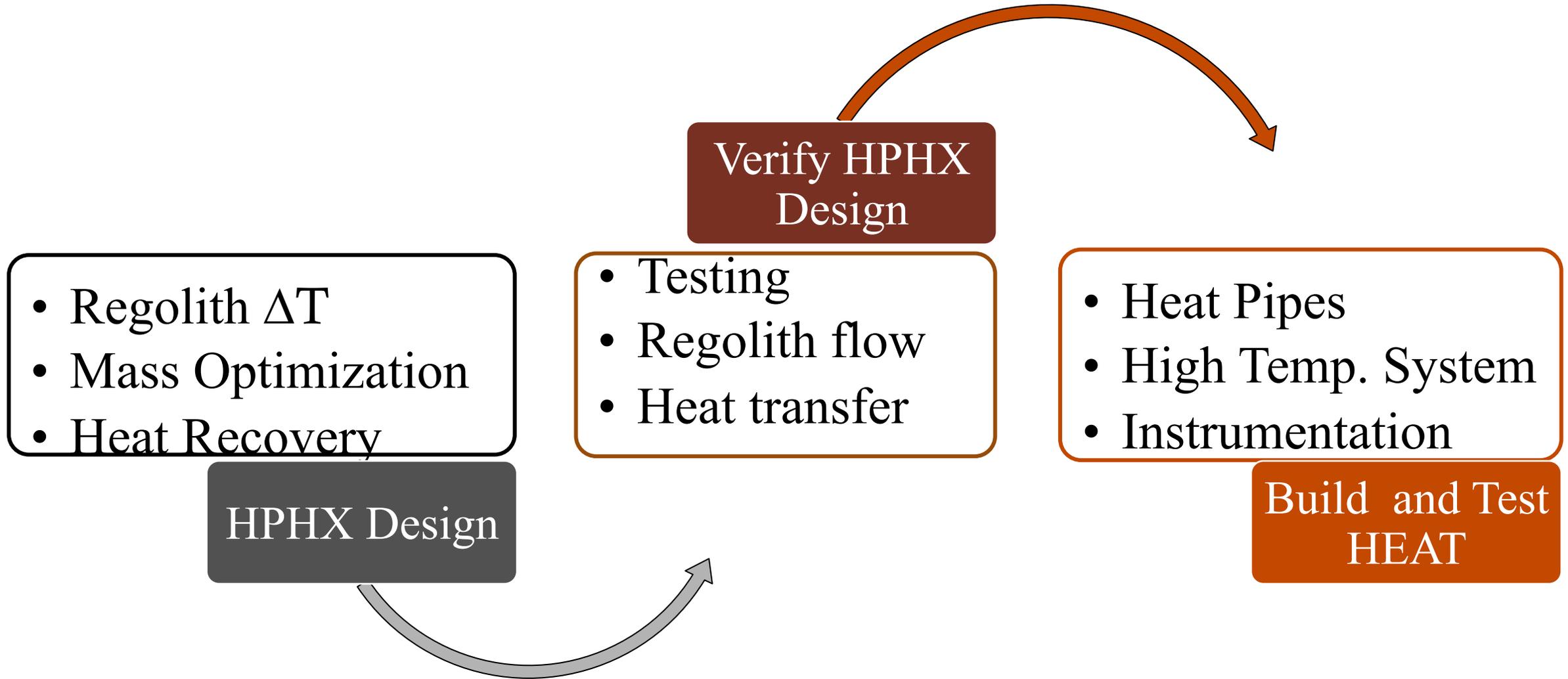
Interest in Lunar Exploration is Ramping Up

Lunar Mission Manifest

Launch Date	Organization	Country	Mission
2015-2018	Google Lunar XPrize (GLXP)		GLXP
2017	CNSA	China 	Chang'e-5
2017	JAXA	Japan 	SELENE-2
2018	ISRO	India 	Chandrayaan-2
2018	NASA	USA 	RP
2018	NASA	USA 	EM-1
2020	CNSA	China 	Chang'e-6
2021	NASA	USA 	EM-2
2020s	Roscosmos	Russia 	Luna-25
		Russia 	Luna-26
		Russia 	Luna-27
		Russia 	Luna-28
		Russia 	Luna-29
JAXA	Japan 	SELENE-3	



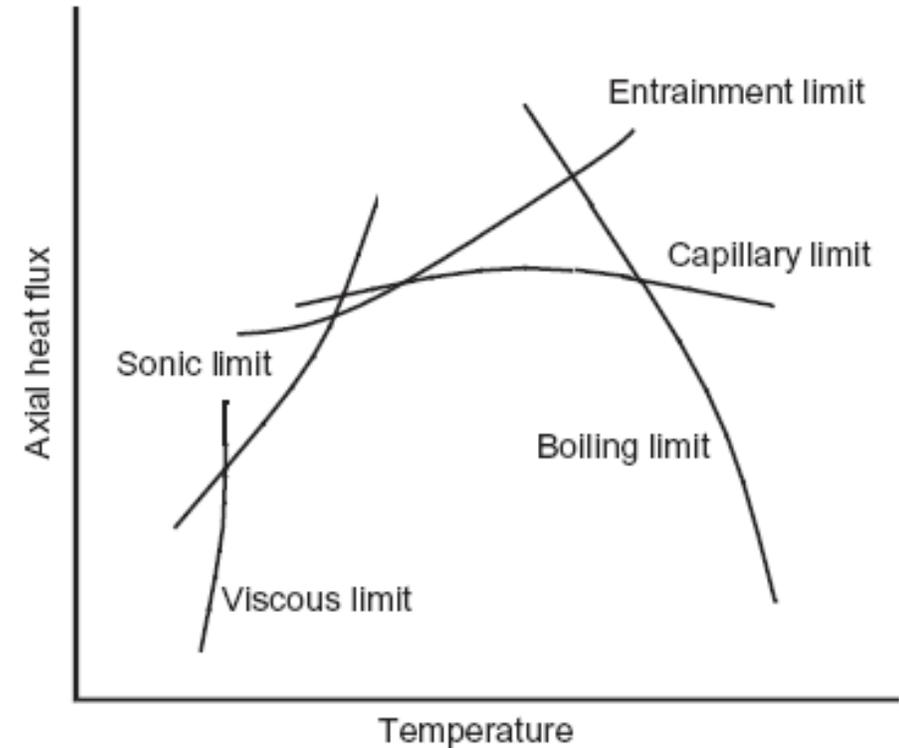
There are Three Key Steps for HEAT



HPHX Design: Heat Pipe Design Considerations

Temperature Range (°C)	Working Fluid	Vessel Material
5-230	Water	Copper, Cu-Ni alloys
190-550	Mercury	Stainless steel
300-600	Cesium	Nickel, Ni-Cr alloys
400-800	Potassium	Stainless steel, Nickel
500-900	Sodium	Stainless steel, Nickel

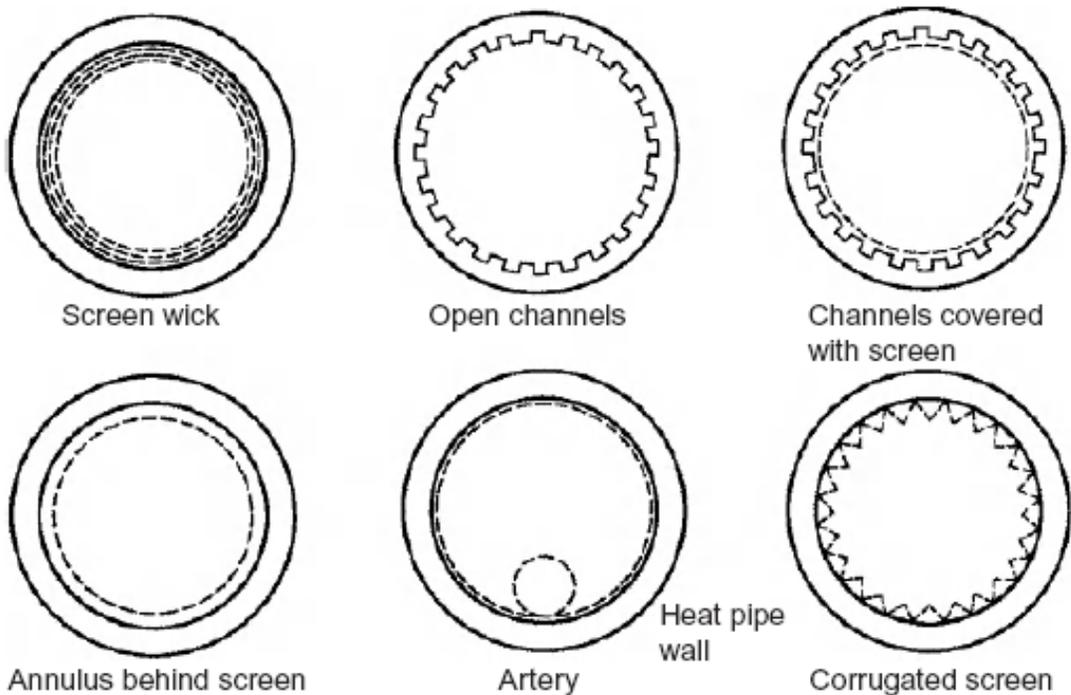
Heat Pipe Limit	Description
Capillary	Capillary pressure of the wick cannot overcome the pressure drops
Viscous	Vapor flow is inhibited by viscous forces at the inner wick surface
Sonic	The vapor velocity maxes out at Mach 1 (speed of sound)
Entrainment	The prevention of liquid return flow
Boiling	Film boiling starts at the evaporator section



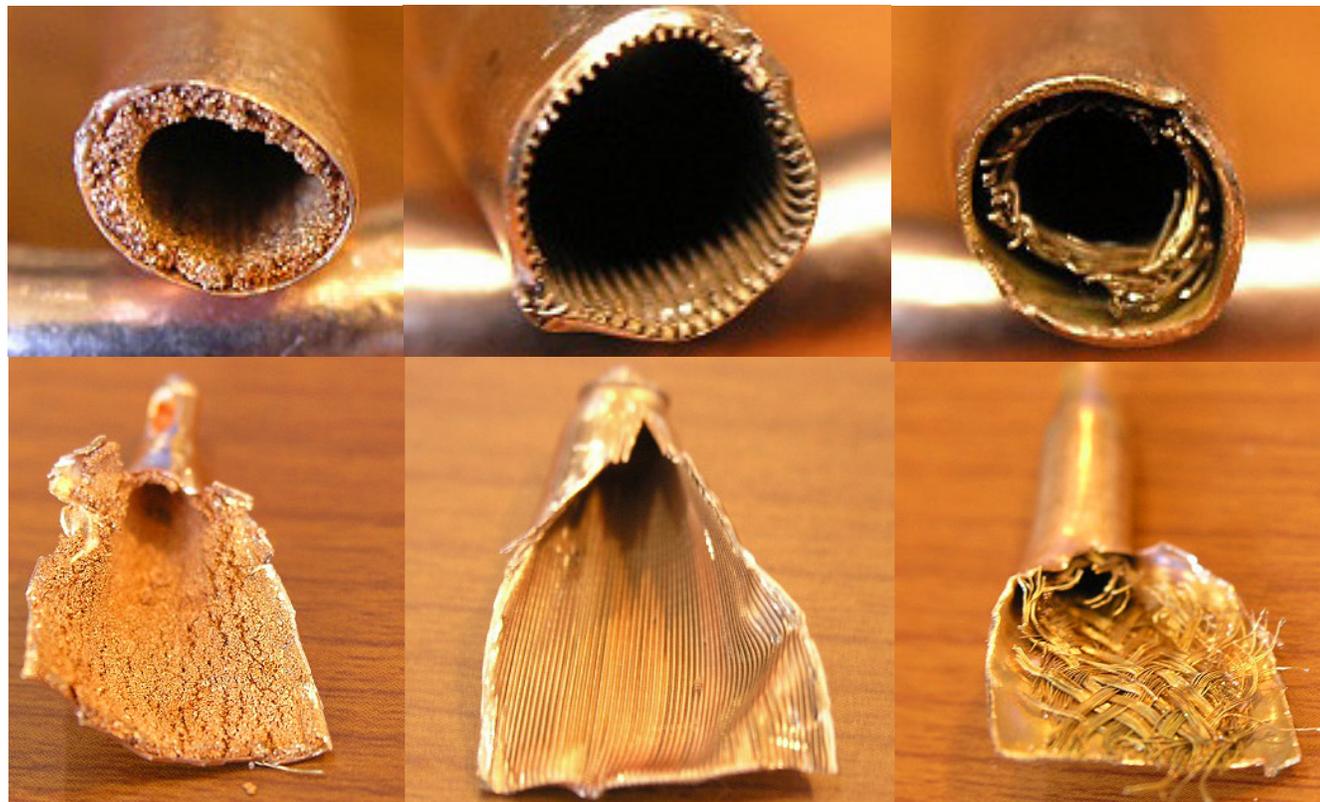
Credit: D.Reay (Heat Pipes, 2005)

HPHX Design: Heat Pipe Design Considerations

- Heat pipe wick to be determined, there are a number of options



Credit: D.Reay (Heat Pipes, 2005)



Credit: Thermolab



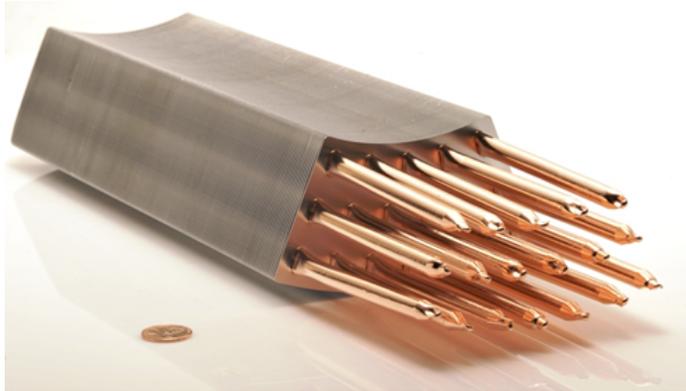
HPHX Design: Three Heat Pipe Manufacturers Identified



Credit: ACT



Credit: ACT



Credit: Thermacore

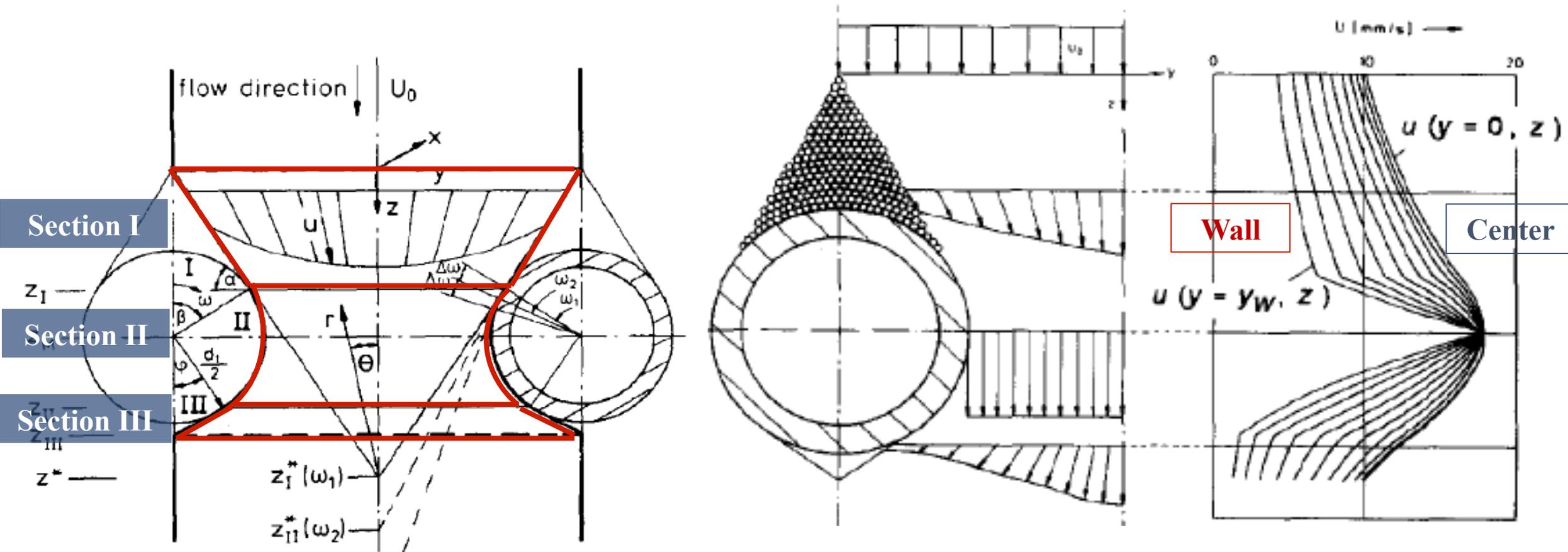


Credit: ACT



HPHX Design: Moving Bed Velocity Field Solution

- Steady 2D flow, material is described as an isotropic, incompressible continuum fluid

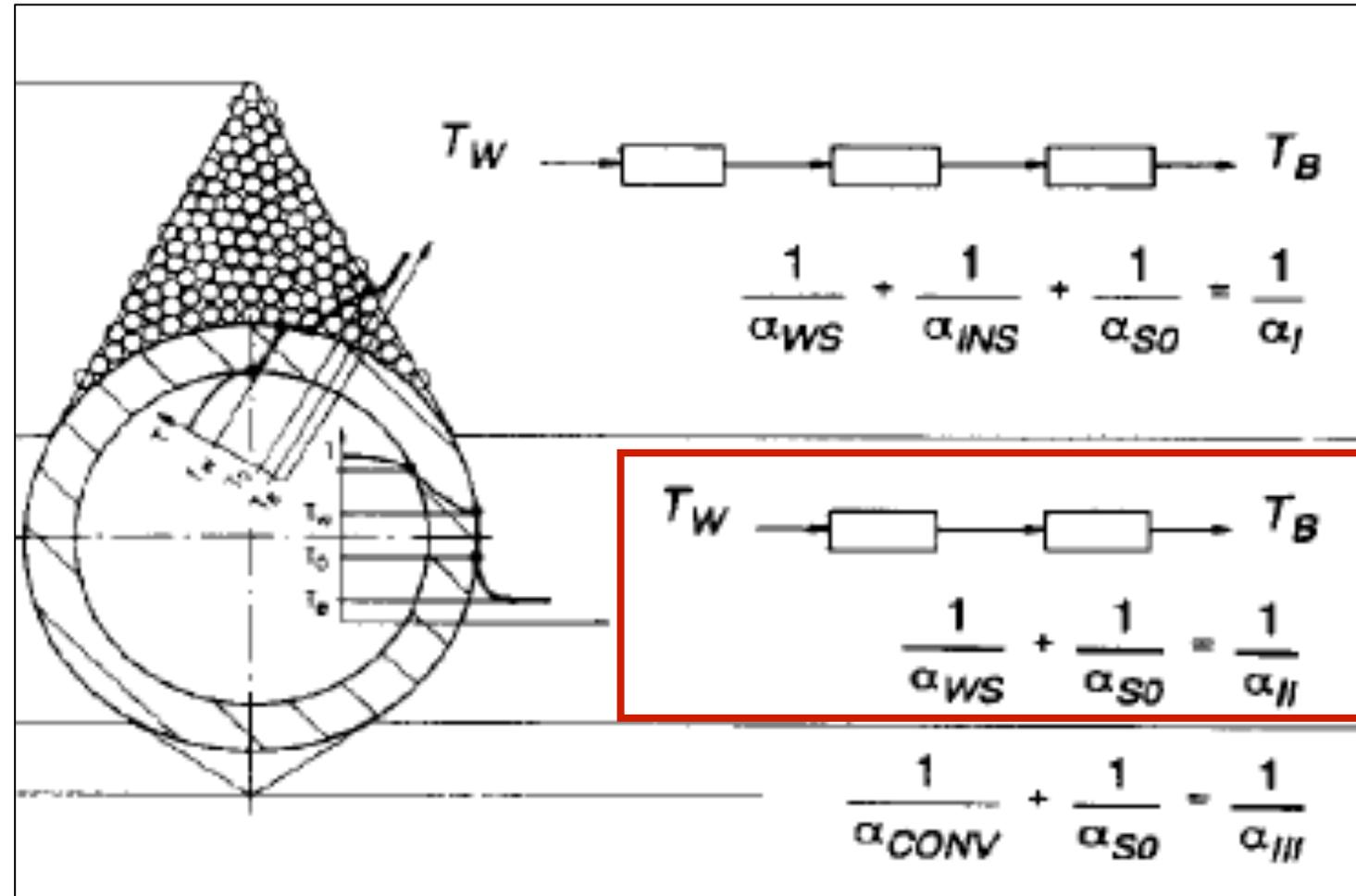


Credit: Niegsch et al.,1994

Credit: Niegsch et al.,1994

HPHX Design: Moving Bed Heat Transfer

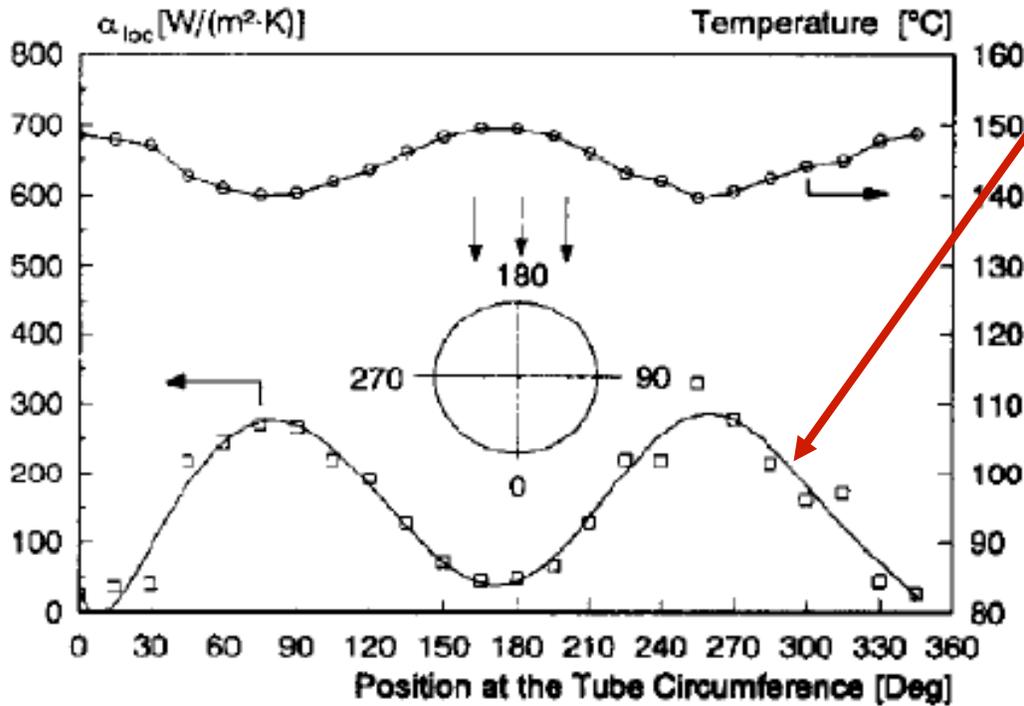
- Thermal resistances vary by section
- Section II has the greatest influence
- Surface heat transfer coefficient
- Heat penetration into the bulk



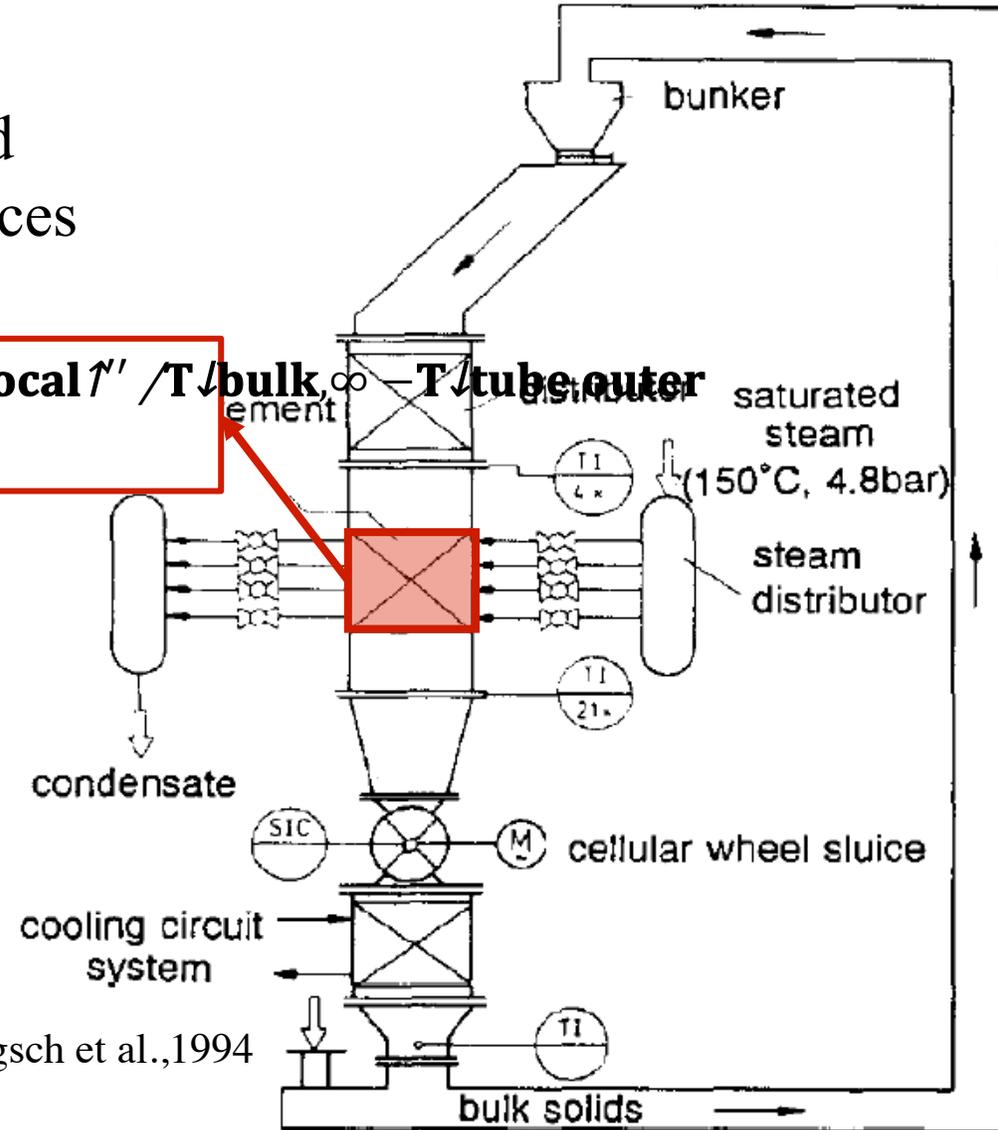
Credit: Niegsch et al., 1994

HPHX Design: Moving Bed Experimental Results

- Niegsch Model matches experimental results
- Heat transfer coefficients measured with a steam heated tube with thermocouples on its inside and outside surfaces



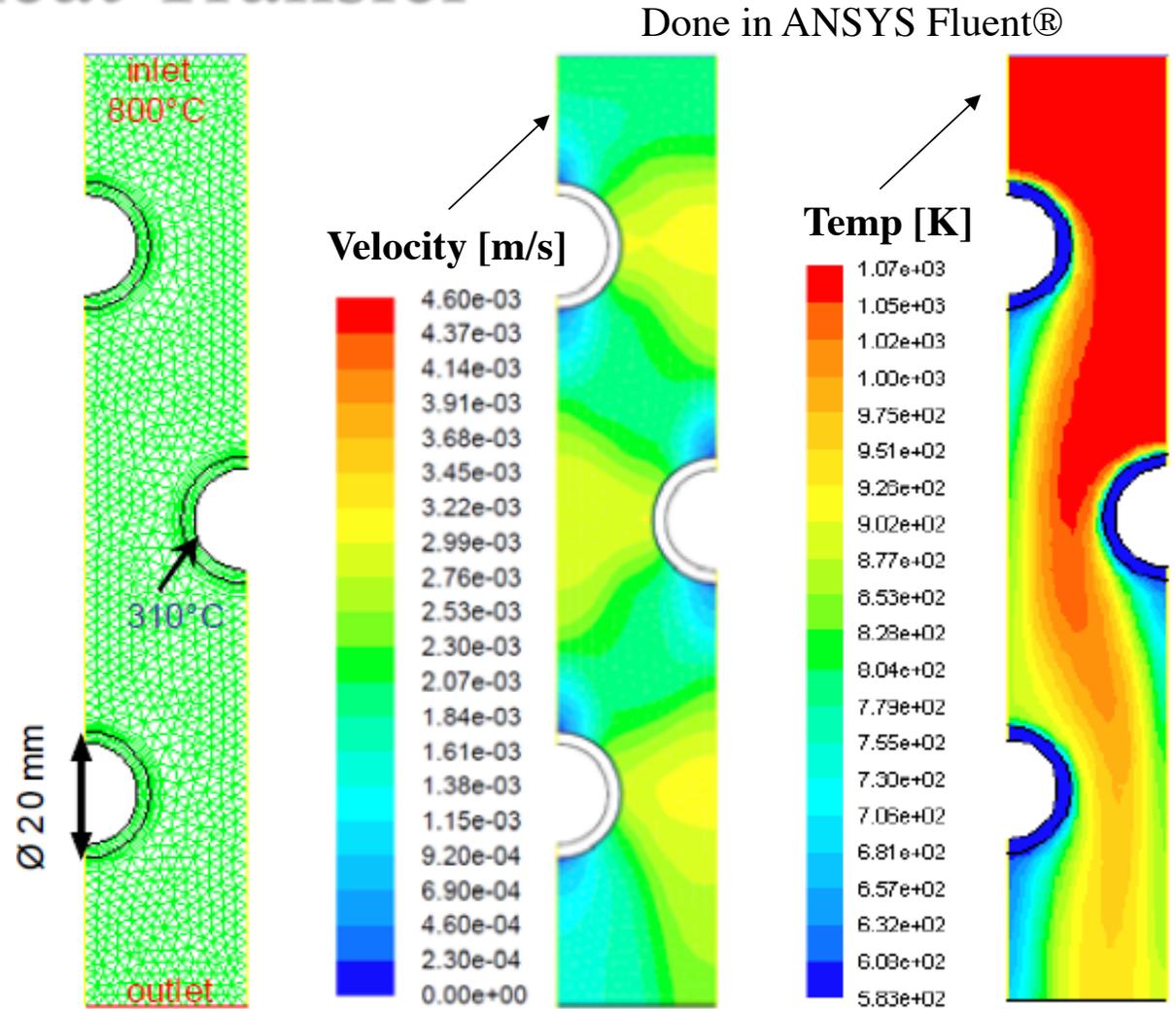
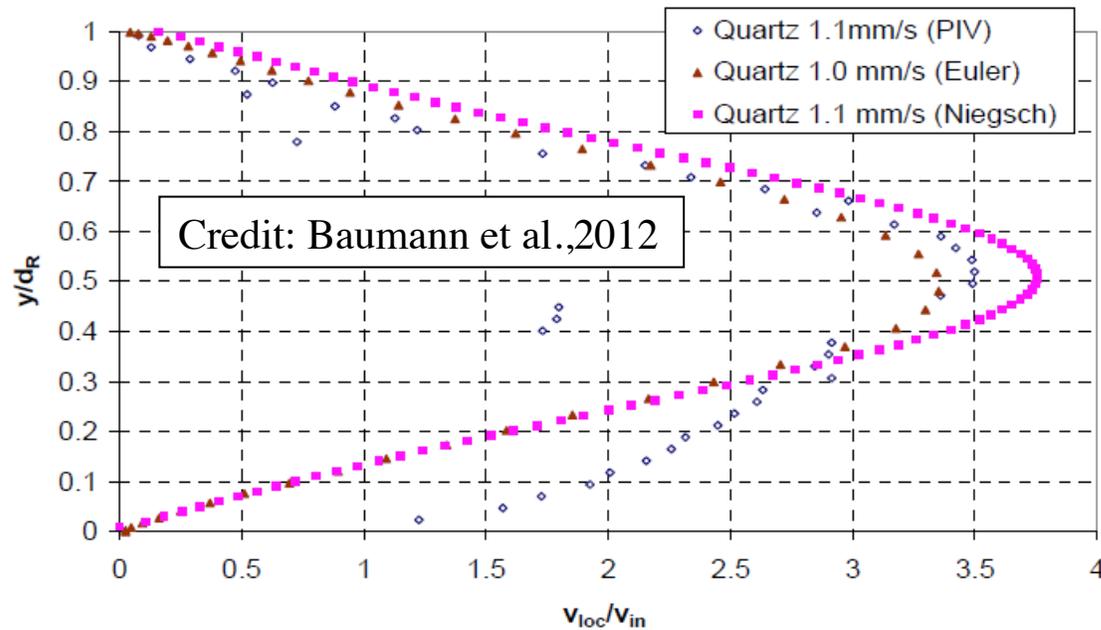
$$h_{local} = q_{tube,local} / (T_{bulk,element} - T_{tube,outer})$$



Credit: Niegsch et al., 1994

HPHX Design: CFD Can Effectively Describe Moving Bed Flow and Heat Transfer

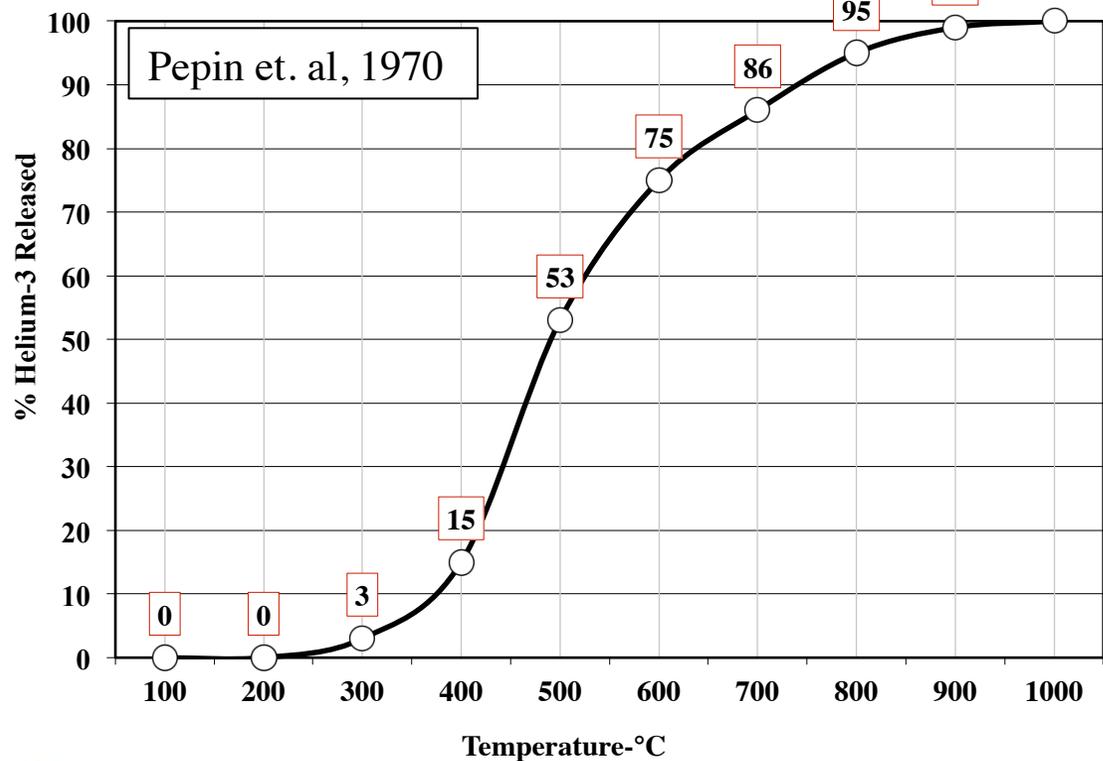
- Euler-Euler Two Phase Granular CFD models match Niegsch results closely
- Particle Image Velocimetry (PIV) used to check against Niegsch model



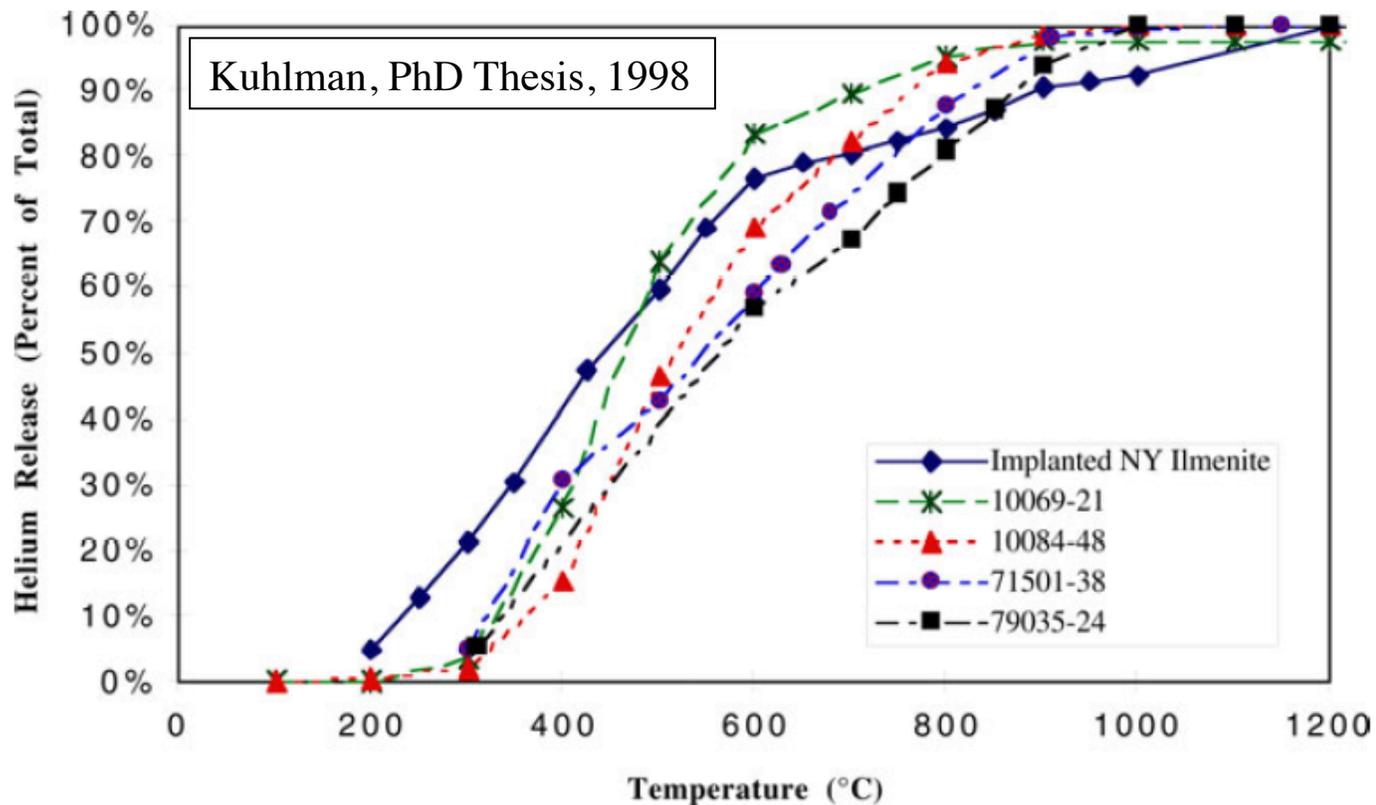
Credit: Baumann et al., 2014

^3He Diffusion out of Lunar Regolith has been Studied

Lunar Regolith



Analog Regolith



HPHX Design: Analysis Simplifications

- Simplifications
 - Effectiveness ratio of unity
 - Capacitance ratio of unity

Stage effectiveness

$$\epsilon_{st} = 2\epsilon/N - (N-1)\epsilon$$

Stage temperature

$$T_p = (T_{hi} + T_{ci}) / 2$$

Stage change in temp. of regolith

$$\Delta T_{st} = \epsilon_{st} (T_p - T_{ci}) = \epsilon_{st} (T_{hi} - T_p)$$

Heat pipe power

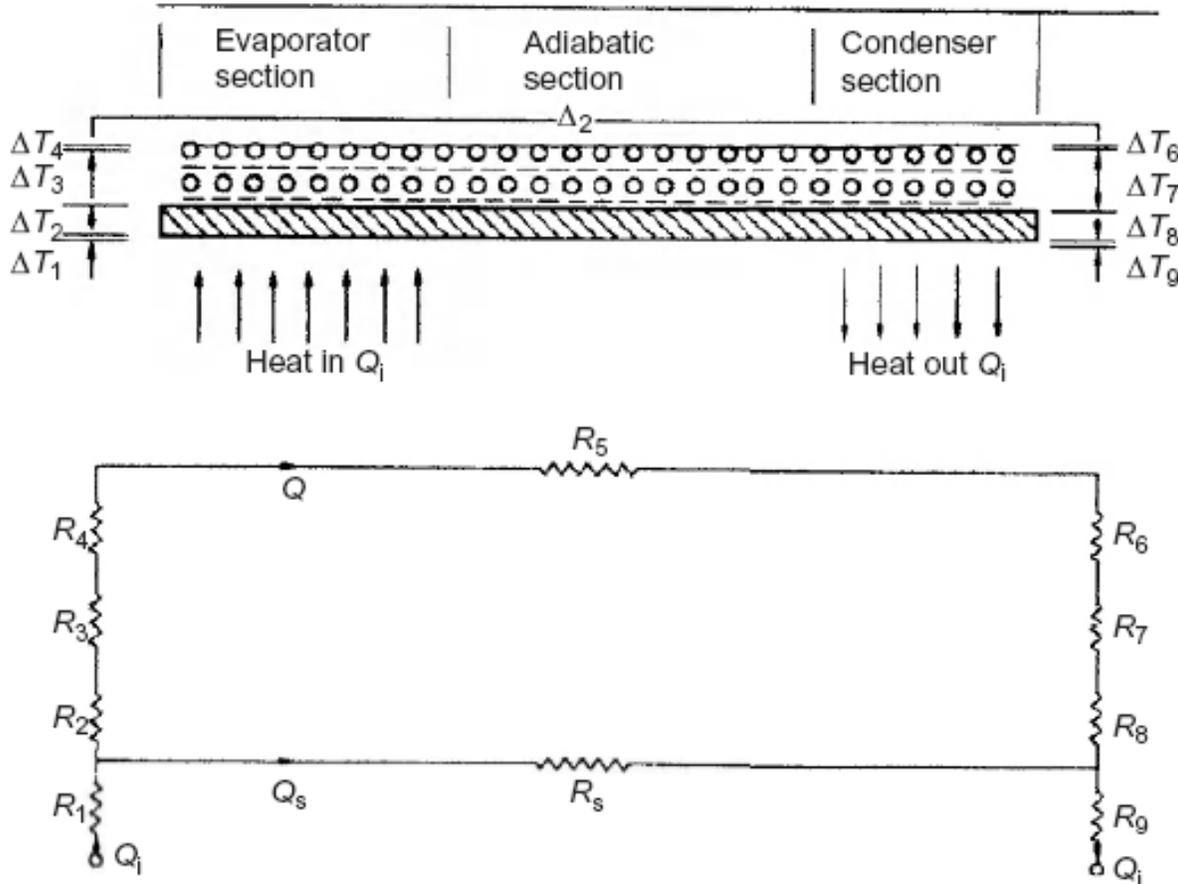
$$Q = C \epsilon_{st} \Delta T_{st} / N_{columns}$$

Total surface area

$$A_t = N A_{st} = N (A_h + A_c) = N C (NTU_s) (1 + h_h / h_c) / h_h$$



HPHX Design: Heat Pipe Thermal Resistances



Credit: D.Reay (Heat Pipes, 2005)

- Heat pipes operate nearly isothermally
 - Temperature variation will have some effect on the overall HX

Thermal Resistance	Description	Typical order of magnitude (Kcm^2/W)
R1	Evaporator external surface area resistance	0.001-10
R2, R8	Heat pipe wall resistance	~ 0.1
R3, R7	Wick structure and liquid conduction resistance	~ 10
R4, R6	Vapor-liquid surface resistance	$\sim 10^{-5}$
R5	Vapor column resistance	$\sim 10^{-8}$
R _s	Heat pipe axial structure resistance	Usually neglected

Overview of lunar simulants

Simulant(s)	Type	Primary Reported Use	Manufacturer	feedstock	status
NU-LHT series	Highlands	General	NASA-MSFC and USGS	Stillwater mine (MT), commercial minerals	In production and use
OB-1	Highlands	Geotechnical	Norcat	Shawmere anorthosite, olivine slag glass	In production and use
JSC-1 (-1A, -1AF)	Mare, low-Ti	Geotechnical and lesser chemical	Orbitec, Inc.	Basalt ash, San Francisco volcanic field (AZ)	In production and use
FJS-1	Mare, low-Ti	Geotechnical	Japanese, (JAXA, LETO)	Mt. Fuji area basalt	No longer available
MLS-1	Mare, high-Ti	Chemical	University of Minnesota	Basalt sill, Duluth complex	No longer available



^3He on the Moon Could Become Extremely Valuable

One of yesterday's U. S. shuttles could return a "payload" worth over \$100 billion in energy.



One of today's SpaceX Dragon capsules could return a "payload" worth around \$15 billion in energy.



40 Tonnes (12 Dragon capsules) of Helium-3 Could Provide all the Electricity Used in North America in 2014



The ^3He on Earth is Insufficient to Support Fusion Power

Three sources of helium-3 on the Earth

- **Atmosphere:**
 - helium-3 concentration in atmosphere is $\approx 7 \times 10^{-12}$ by volume.
 - total amount in the entire atmosphere is $\approx 4,000$ tonnes
- **Natural Gas:** potentially as much as 280 kg in reserves and speculative sources that are not being tapped
- **Decay of Tritium:** tritium decays into helium-3 with a 12.3 year half life and 2-4 kg/yr of helium-3 is produced from tritium in the U.S. and Canada

Shortage

- **Increased Usage:** supply depleted of helium-3 from tritium decay (down to < 10 kg in the U.S. as of 2010)
- **Increased Price:** from ($\sim \$1,000,000/\text{kg}$) to ($> \$30,000,000/\text{kg}$)
- **Available for Fusion R&D:** only ~ 10 kg ^3He (200 MW-y fusion energy) is accessible on Earth

Exhibit Earns First Place at the 2015 UW Engineering Expo

- Over 10,000 students and parents visited
- Graduate/group category
- Thank you to Abe Megahed for miner simulation work

